TECHNICAL AND APPLICATION GUIDE
AKD-20
Low voltage switchgear



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## Warranty and general information

## Hazard classifications

The following important highlighted information appears throughout this document to warn of potential hazards or to call attention to information that clarifies a procedure.

Carefully read all instructions and become familiar with the devices before trying to install, operate, service or maintain this equipment.

Danger: Indicates a hazardous situation which, if not avoided, will result in death or serious injury.

Warning: Indicates a hazardous situation that, if not avoided, could result in death or serious injury.

Caution: Indicates that if the hazard is not avoided could result in minor or moderate injury.

Notice: Is used to notify of practices not related to personal injury.

## Trademarks

EntelliGuard ${ }^{\circledR}$ G
EntelliGuard ${ }^{\circledR}$ TU
Arc Vault ${ }^{\text {TM }}$ Protection System

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## Warranty

This document is based on information available at the time of publication. While efforts have been made to ensure accuracy, the information contained herein does not cover all details or variations in hardware and software, nor does it provide for every possible contingency in connection with installation, operation, and maintenance. Features may be described herein that are not present in all hardware and software systems.

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No warrantees of merchantability or fitness for purpose shall apply. Contact your local sales office if further information is required concerning any aspect of AKD-20 switchgear and EntelliGuard G breaker operation or maintenance.

## AKD-20 <br> General information

AKD-20 low voltage switchgear continues many of the traditions of the AKD switchgear lines while delivering new benefits, including:

- Enhanced arc flash protection;
- Smaller and lighter power circuit breakers;
- Higher interrupting ratings without the use of fuses;
- Smaller footprints associated with the higher ratings.

They're all part of the AKD-20 and EntelliGuard standard product offering. AKD-20 switchgear is manufactured in an ISO9002 certified ABB facility and built to the highest standards.

AKD-20 switchgear meets the demands of industrial, utility and commercial applications. It is designed and tested in accordance with the latest IEEE C37.20.1 standard, IEEE C37.20.7 arcresistant standard, CAN/CSA-C22.2 No. 31, and UL 1558 standards (file no. E76012). AKD-20 has been conformance-tested to ANSI C37.51. Any equipment requiring UL 1558 or CSA labeling will be provided with a cUL label. (A cUL label is a third-party certification that indicates the switchgear is compliant to both ANSI/IEEE and CSA standards.)

ANSI standards require that switchgear operates at the ratings of devices installed. Switchgear short circuit ratings are based on two 30-cycle withstand tests with 15 -second interval, performed at $15 \%$ power factor and 635 Vac maximum. For switchboards, a single 3-cycle withstand test at $20 \%$ power factor and 600 Vac maximum is performed.

AKD-20 switchgear is available with the ollowing ratings:

- 600 Vac nominal, 635 Vac maximum;
- 8000 amps AC main bus/6000 amps breaker max.;
- $50 / 60 \mathrm{~Hz}$;
- 150 kA symmetrical short circuit;
- 2200 Vac rms dielectric.

AKD-20 switchgear breaker and auxiliary sections are constructed with 11-gauge frames and are furnished in $22^{\prime \prime}, 30^{\prime \prime}, 34^{\prime \prime}$ and $38^{\prime \prime}$ widths. The switchgear is designed to be operated in ambient temperatures between $-30^{\circ} \mathrm{C}$ and $40^{\circ} \mathrm{C}\left[-22^{\circ} \mathrm{F}\right.$ and $104^{\circ} \mathrm{F}$ ].

Low voltage circuit breakers rated 800/1600/ 2000 amps can be stacked in four-high combinations resulting in reduced floor space requirements. The 11-gauge, bolted modular-designed steel frame permits flexibility in arrangements of breakers and associated components.

AKD-20 switchgear houses low voltage power circuit breakers, instrumentation, and other auxiliary circuit protective devices in single or multiple source configurations. AKD-20 switchgear can be applied either as a power distribution unit or as part of a unit substation in indoor or outdoor construction.

The breaker cubicles use cassette-type construction. A metal breaker cassette is incorporated into the breaker cubicle and includes the drawout mechanism, safety interlocks, and provisions for accessories such as shutters, position switches, secondary disconnects, and key interlocking.

The new EntelliGuard G low voltage power circuit breaker (LVPCB) offers every advantage of the traditional ironframe LVPCB while being smaller and lighter. The circuit breaker's frames have continuous current ratings from 800 A to 6000 A and sensors from 400 A to 6400 A, with rating plug values as low as 150 A . Short-circuit ratings are available up to 150 kA , with $65 \mathrm{kA}, 85 \mathrm{kA}$, and 100 kA 30-cycle withstand ratings to match.

The EntelliGuard TU electronic trip unit family - with its unique waveform recognition instantaneous algorithm and the industry's only true Instantaneous Zone Selective Interlocking (I-ZSI) - provides unsurpassed flexibility, selectivity, and arc flash protection. EntelliGuard TU enables entire power distribution systems to be designed with $100 \%$ instantaneous protection in switchgear mains or feeders to achieve a reliable power distribution system. AKD-20 low voltage switchgear, EntelliGuard G LVPCB, and EntelliGuard TU trip units.

Standard and optional features - for enhanced operation and reliability

## Cassette construction

AKD-20 switchgear has several key components that set it apart from previous ABB low voltage switchgear designs. The EntelliGuard $G$ breaker fits into a metal cassette built in to the circuit breaker cubicles, as shown in Figure 1-1. AKD- 20 breaker cubicle construction uses an unventilated front door that provides closed-door access to breaker status indicators, mechanism operators, trip unit display and keypad, and it allows for closed-door drawout operation.


Figure 1.1: Cassette construction

The breaker cubicle door has a standard quarter-turn latch and serves as a steel barrier between live parts and the operator. The cassette houses accessories as well as interlocks for the drawout breaker. Accessories include current transformers for discrete metering or relaying, drawout position switches, shutters, and key interlocks.

## Repetitive duty

Circuit breakers are designed primarily to perform the function of circuit interruption under short-circuit conditions.

Nevertheless, modern circuit breakers' mechanisms are capable of many operations under full-load operation and in-rush conditions such as those encountered in motor starting applications. Industry standards have been established for the minimum performance, as indicated in Table 1.1. With adequate maintenance, EntelliGuard G/E can be expected to exceed the standards.

EntelliGuard breakers have been designed and tested to allow the user to extend the normal maintenance service interval up to two times the ANSI recommendation - a significant benefit for continuous process and 7-X-24 operations. See Table for additional information.

Power-operated circuit breakers, when operating under usual service conditions, shall be capable of operating the number of times specified in the following table. The operating conditions and the permissible effect of such operations upon the breaker are listed in Table and the footnotes. For instance, the breaker should be operated with rated control voltage applied. The frequency of operation should not exceed 20 in 10 minutes or 30 in an hour (rectifiers or other auxiliary devices may further limit the frequency of operation).

Servicing consisting of adjusting, cleaning, lubricating, tightening, etc., as recommended by the maintenance manual, is to be done at no greater interval than shown in the column titled "Number of operations between servicing" in Table.

No functional parts should require replacement during the listed operations. The circuit breaker should be in condition to carry its rated continuous current at rated maximum voltage and perform at least one opening operation at rated shortcircuit current. After completion of this series of operations, functional part replacement and general servicing may be necessary. This standard applies to all parts of a circuit breaker that function during normal operation. It does not apply to other parts, such as overcurrent tripping devices that function only during infrequent abnormal circuit conditions.

Table 1.1: Repetitive duty and normal maintenance (from ANSI C37.16 table 5)

| Circuit breaker <br> frame size (amperes) | Number of operations <br> between servicing | Number of operations <br> rated continuous current <br> switching ${ }^{(1)(2)(4)}$ | Number of operations <br> on-load closing and <br> opening ${ }^{(1)}$ | Number of operations <br> in-rush current <br> switching |
| :--- | ---: | ---: | ---: | ---: |
| 800 | 1750 | 2800 | 9700 | 1400 |
| 1600 | 500 | 800 | 3200 | 400 |
| 2000 | 500 | 800 | 3200 | 400 |
| 3200 | 250 | 400 | 1100 | - |
| 4000 | 250 | 400 | 1100 | - |
| 5000 | 250 | 400 | 1100 | - |

[^0]
## Temperature derating factors

The continuous current rating of EntelliGuard breakers is based on their use in an enclosure at $40^{\circ} \mathrm{C}$ ambient temperature and $105^{\circ} \mathrm{C}$ maximum breaker temperature for Class A tings of EntelliGuard breakers must be derated for ambient temperatures above $40^{\circ} \mathrm{C}$. (Trip unit ambient is limited to $70^{\circ} \mathrm{C}$.)

Table 1.2: Continuous current derating factors

| Ambient temperature $\left({ }^{\circ} \mathrm{C}\right)$ | Derationg factor |
| :--- | ---: |
| 40 | 1.00 |
| 45 | 0.95 |
| 50 | 0.89 |
| 55 | $0.84^{(1)}$ |
| 60 | 0.77 |
| 65 | 0.71 |
| 70 | 0.63 |

1. Trip unit maximum

## Altitude correction factors

When applying low voltage power circuit breakers at altitudes greater than 6,600 feet, their continuous current rating must be modified because a higher temperature use will be experienced for a given current rating. The voltage ratings must also be modified because of the lower dielectric strength of the air. The short-time and short-circuit current ratings are not affected by altitude. However, the short-circuit current ratings shall not exceed that of the voltage class before derating.

Table 1.3: Altitude correction factors
(as listed in ANSI C37.13)

| Altitude |  | Rating correction factor |  |
| :--- | :--- | :--- | :--- |
| Meters | Feet | Continuous <br> current | Voltage |
| 2000 | 6600 (and below) | 1.00 | 1.00 |
| 2600 | 8500 | 0.99 | 0.95 |
| 3900 | 13000 | 0.96 | 0.80 |

## Humidity

Ferrous parts are zinc-plated for corrosion protection except for some parts made from alloy steels that are inherently corrosion resistant. Current-carrying parts are silver- or tinplated for corrosion protection and to assure electrical continuity. Heaters may be added to indoor sections operating in high humidity environments. Heaters are mounted in the bus/cable compartment in the rear of each section.

Table 1.4: Insulation values (dielectric test)

|  | kV |
| :--- | :---: |
| Breaker | 2.2 |
| Control wiring | 1.5 |
| Closing motor | 0.9 |

Table 1.5: Breaker operating time (same for all frame sizes)

| Close (time from <br> energizing closing <br> circuit until <br> contacts touch) | Electrically operated | 5 Cycles |
| :--- | ---: | ---: |
| Open (maximum <br> clearing time) | With instantaneous <br> overcurrent trip | 3 Cycles |
|  | With shunt trip | 3.5 Cycles |

## Primary disconnect shutters

Optional shutters (Figure 1.2) can be specified for all breaker cubicles. An insulated cam opens the shutters when the breaker is racked in from the TEST position to the CONNECT position. The shutters close when the breaker is between the TEST and DISCONNECT positions. They can be locked in the closed position (Figure 1.3) when the breaker is removed from the cubicle, preventing access to the line and load stabs in the breaker cubicle. Shutters are provided as a standard feature for source and tie breakers on switchgear lineups with multiple sources. These applications include main-tie-main or main-generator lineups. Shutters for feeder breakers are optional in multisource lineups.

-
Figure 1.2: Primary disconnect shutters (open and closed positions, respectively)


Figure 1.3: Primary disconnect shutters (locked in the closed position)

## Kirk key interlocks

Key interlocks can be added to the cassette to mechanically lock the breaker open, in a trip-free position, when the breaker is in the CONNECT position (Figure 1.4).

The cassette will accommodate either one or two Kirk key interlocks. Interlocking schemes prevent multiple breakers from being closed at the same time, such as a utility main and emergency generator, or preventing a tie breaker from being closed until a main circuit breaker is opened. Key interlocks are also used to prevent operation of a transformer primary switch unless the main secondary breaker is open. Key interlocks mounted in the breaker cassette stay with the breaker cubicle so that the interlock scheme is maintained even if a spare breaker is inserted into a main, tie, or generator breaker cubicle. Key interlocks also prevent breaker racking into any other position when engaged. Proper breaker position (CONNECT, TEST, or DISCONNECT) must be selected before engaging the key interlock.


Figure 1.4: Kirk keys locking breakers (breaker in the CONNECT position)

## Breaker rating rejection

The cassette also includes rating interlocks to prevent a breaker of incorrect short-circuit rating or continuous current rating from being installed into a cassette (Figure 1.5). There are three physical envelope sizes for the EntelliGuard G breaker. The physical size differences will not allow breakers of a different envelope size to fit into an incorrect compartment. Within an envelope size, a breaker with a higher short circuit rating will fit into a lower rated cassette if the continuous current rating of the breaker is less than or equal to the rating of the cassette.

As an example, an 800 A, 85 kA interrupting breaker can be installed into a 1600 A, 65 kA breaker cassette. However, a 1600 A breaker cannot be installed into an 800 A cassette, nor can a 65 kA breaker be installed into an 85 kA cassette.


Figure 1.5: Breaker and cassette rejection (respectively)


## Cassette interlocks

Drawout interlocks are part of the cassette and prevent the breaker from being moved into or out of the CONNECT position unless the circuit breaker is open (Figure 1.6). The interlocks also prevent closing a breaker unless it is in the fully CONNECT or TEST position. A spring discharge interlock releases any energy stored in the closing springs when the circuit breaker is removed from the cassette.


Figure 1.6: Drawout interlocks

## Padlocking provisions

Several types of padlocking provisions are standard on the cassette and breaker. The cassette has provisions for padlocking the shutters in the closed position (Figure 1.3) and for padlocking access to the racking mechanism (Figure 1.7).

The drawout rails have provisions for up to three padlocks to prevent a circuit breaker from being installed into the cassette (Figure 1.8). The circuit breaker has provisions for up to three padlocks that will keep the breaker open and mechanically trip free (Figure 1.9).

An optional padlockable cubicle quarter-turn latch is available unauthorized access to the breaker cubicle.


[^1]

Figure 1.8: Drawout rail padlocked (and close-up)


Figure 1.9: Breaker padlocked

## Door interlock

An optional door interlock can be supplied on the cassette to automatically secure the breaker cubicle door and prevent entry into the breaker cubicle unless the circuit breaker is racked out to the TEST or DISCONNECT position.

## Instrument panel

Standard construction includes a grounded steel instrument panel above each circuit breaker (Figure 1.10). This panel is used for mounting a variety of control circuit components - including fuses for the charge, close, and trip circuits; indicating lights, and the Reduced Energy LetThru switch. Control circuit fuses and indicating lamps are replaceable from the front of the panel. The panel is removable to provide access to wiring terminations. An engraved circuit nameplate is also provided on each breaker cubicle instrument panel.


Figure 1-10: Instrument panel with RELT switch

## Secondary disconnects

Breaker control circuit devices and trip unit inputs and outputs are connected to the breaker through secondary disconnects mounted on the front of the breaker and cassette (Figure 1.11). This provides convenient access to the secondary control terminal points for monitoring or troubleshooting.


Figure 1.11: Secondary disconnects

All breaker-mounted accessories have dedicated wiring points on the secondary disconnects. Adding accessories to the breaker requires only plugging the wire harness, included with the accessory, into the open points on the secondary disconnect.

## Current transformers

Relaying class CTs can be supplied for Envelope 1, 2, and 3 breakers. The relaying class CTs are located in the breaker cassette and are mounted on the three upper primary disconnect stabs in the cubicle. Up to three relaying current transformersmay be mounted in the breaker cubicle. CT ratios, associated relaying class, and internal winding resistance are shown in Table 1.6, Table 1.7, and Table 1.8.

Relaying class CTs are used for ground fault protection on four-wire, double-ended switchgear applications. The relaying CTs indicated in Table 1.6, Table 1.7, and Table 1.8 are suitable for use with equivalent main and tie breaker ampere ratings. A detailed description of the 4 - wire ground fault system is provided on page 63 (Figure 3.1).

Table 1.6: AKD-20 Envelope 1 relaying current transformers

| Current ratio | Relay class | ANSI metering class @60 Hz |  |  |  |  | Secondary winding resistance (Ohms @75 ${ }^{\circ} \mathrm{C}$ ) | $\begin{array}{r} \text { Cat } \\ \text { \#0173B4776 } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | B0. 1 | B0.2 | B0.5 | B0.9 | B1.8 |  |  |
| 100:5 | - | 2.4 | 1.2 | - | - | - | 0.0313 | P001 |
| 150:5 | - | 1.2 | 1.2 | - | - | - | 0.0236 | P002 |
| 200:5 | - | 0.6 | 1.2 | 2.4 | - | - | 0.0651 | P003 |
| 250:5 | C10 | 0.6 | 0.6 | 2.4 | 2.4 | - | 0.0460 | P004 |
| 300:5 | C10 | 0.3 | 0.6 | 1.2 | 2.4 | - | 0.0760 | P005 |
| 400:5 | C20 | 0.3 | 0.3 | 0.6 | 1.2 | 2.4 | 0.1063 | P006 |
| 500:5 | C20 | 0.3 | 0.3 | 0.6 | 1.2 | 1.2 | 0.1394 | P007 |
| 600:5 | C20 | 0.3 | 0.3 | 0.3 | 0.6 | 1.2 | 0.1509 | P008 |
| 750:5 | C20 | 0.3 | 0.3 | 0.3 | 0.3 | 0.6 | 0.1858 | P009 |
| 800:5* | C20 | 0.3 | 0.3 | 0.3 | 0.3 | 0.6 | 0.2091 | P010 |
| 1000:5* | C20 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.2673 | P011 |
| 1200:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3480 | P012 |
| 1500:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3948 | P013 |
| 1600:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4180 | P014 |
| 2000:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.5109 | P015 |

* Indicated relaying CTs may be used for ground fault protection on main and tie breakers in four-wire, double-ended switchgear applications

Table 1.7: AKD-20 Envelope 2 relaying current transformers

| Current ratio | Relay <br> class | ANSI metering mlass @60 Hz |  |  |  |  | Secondary winding resistance (Ohms @75 ${ }^{\circ} \mathrm{C}$ ) | $\begin{array}{r} \text { Cat } \\ \text { \#0173B4776 } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | B0.1 | B0.2 | B0.5 | B0.9 | B1.8 |  |  |
| 100:5 | - | 2.4 | 2.4 | - | - | - | 0.03356 | P001 |
| 150:5 | C10 | 2.4 | 2.4 | - | - | - | 0.03830 | P002 |
| 200:5 | C10 | 0.6 | 1.2 | 2.4 | 2.4 | - | 0.04760 | P003 |
| 250:5 | C10 | 0.6 | 1.2 | 1.2 | 2.4 | 2.4 | 0.09670 | P004 |
| 300:5 | C20 | 0.6 | 0.6 | 1.2 | 1.2 | 2.4 | 0.04350 | P005 |
| 400:5 | C20 | 0.3 | 0.6 | 0.6 | 1.2 | 2.4 | 0.15097 | P006 |
| 500:5 | C50 | 0.3 | 0.3 | 0.6 | 0.6 | 1.2 | 0.18580 | P007 |
| 600:5 | C50 | 0.3 | 0.3 | 0.3 | 0.6 | 0.6 | 0.21136 | P008 |
| 750:5 | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.6 | 0.26710 | P009 |
| 800:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.6 | 0.29030 | P010 |
| 1000:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.36002 | P011 |
| 1200:5* | C100 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.39480 | P012 |
| 1500:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.41810 | P013 |
| 1600:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.42960 | P014 |
| 2000:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.60340 | P015 |
| 2500:5* | C100 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.70840 | P016 |
| 3000:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.65030 | P017 |
| 3200:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.70840 | P018 |

* Indicated relaying CTs may be used for ground fault protection on main and tie breakers in four-wire, double-ended switchgear applications.

Table 1.8: AKD-20 Envelope 3 relaying current transformers

| Current ratio | Relay class | ANSI metering class @60 Hz |  |  |  |  | Secondary winding resistance (Ohms @75 ${ }^{\circ} \mathrm{C}$ ) | $\begin{array}{r} \text { Cat } \\ \text { \#0173B4776 } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | B0.1 | B0.2 | B0.5 | B0.9 | B1.8 |  |  |
| 2000:5 | C100 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.5450 | P001 |
| 2500:5* | C100 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.6387 | P002 |
| 3000:5* | C100 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.7781 | P003 |
| 3200:5* | C100 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.8477 | P004 |
| 4000:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 0.8245 | P005 |
| 5000:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 1.0450 | P006 |
| 6000:5* | C50 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 | 1.7500 | P007 |

* Indicated relaying CTs may be used for ground fault protection on main and tie breakers in four-wire, double-ended switchgear applications.


## AKD-20 Bus Options

AKD-20 bus options are shown in Table 1.9. All horizontal and vertical bus bars (phase, neutral, and ground) are the standard tin-plated copper. Tin plating is desirable for many industrial applications such as wastewater treatment, pulp and paper, petrochemical and other areas where the environment may be damaging to silver plating. Tin-plated bus is also provided as standard for commercial and utility applications. An optional silver-plated bus may be specified for phase, neutral and ground buses. In all applications, the primary disconnect stabs for drawout breakers are provided with full silver plating. Primary disconnect stabs are removable and replaceable in the breaker cassette. Bare copper bus is standard in AKD-20 switchgear, as are insulated runbacks for feeder breakers 2000 A and smaller. Options for insulated horizontal bus, phase-isolated vertical bus, and bus compartment barriers for the phase bus are available as shown in Table 1.9.

When the insulated/ isolated bus option is specified, all main bus joints are covered with an insulating cap so that only the feeder cable terminations are exposed. Bus compartment barriers provide polyester-glass barriers between the bus compartment and the cable compartment. Additional isolation can be provided in the cable compartment of each vertical section by specifying section barriers.

The section barrier option provides a combination of steel and polyester-glass barriers in the rear of each vertical section. The steel barrier provides isolation between sections in the cable termination area, and the polyester-glass barriers provide isolation in the main bus area. When supplied, the section barrier option prevents exposure to the cable terminations in adjacent vertical sections when performing any operations in the rear of a section.

Table 1.9: AKD-20 switchgear bus options

| Main bus rating (A) | 2000 | 3200 | 4000 | 5000 | 6000 | 8000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vertical bus rating (A) |  |  |  | 2000/3200/4000/5000/6000 |  |  |
| Insulated main bus/Isolated vertical bus | - | - | - |  |  |  |
| Bus compartment barriers | - | - | - | - | - | - |
| Section barriers (Rear) | - | - | - | - | - | - |
| Neutral bus rating (A) |  |  |  | 2000/3200/4000/5000/6000 |  |  |
| Ground bus (0.25" $\times 3$ " Cu ) |  |  |  | 1 Bar |  | 2 Bars |
| Short circuit bracing (kA) |  |  |  |  | 65/85/ | 50/200 |
| 30-cycle withstand (kA) |  |  |  |  |  | 85/100 |

## Expansion capabilities

AKD-20 switchgear is designed to be easily expanded to handle increased loading. It is very common, and advisable, to specify "fully equipped future breaker" cubicles when ordering a substation or lineup. The fully equipped future breaker cubicle contains line and load side primary disconnects, cassette with drawout rails and interlocks, and a cubicle door with a cover over the breaker cutout. At time of manufacture, the cubicle can also be outfitted with any specified metering, protection, and control devices, or these can be added when the breaker is installed. Adding a new feeder breaker can then be as simple as removing a cover from the cubicle door and installing the breaker.

Standard bus configurations used in AKD-20 have built-in provisions for future bus extensions. Should the switchgear have no future breaker compartments, additional vertical sections can be mechanically and electrically connected to the AKD-20 lineup without modifications. AKD-20 sections can also be added to existing AKD-8 and AKD-10 equipment. A 2-in. to 8-in. spacer may be required when adding sections to existing equipment.

## IR Windows

Optional Infrared (IR) Scanning Windows (Figure 1.12) can be provided in the switchgear rear covers to facilitate the use of IR cameras for performing thermal scans of cable terminations. Use of the IR windows minimizes exposure to live conductors while performing this preventive maintenance operation. Crystal-type IR windows are used on both indoor NEMA 1 and outdoor NEMA 3R applications. IR windows have a gasketed cover plate secured with tamper-resistant hardware.

Quantity and location of the IR windows are dependent on the breaker stacking arrangement. Typically, one IR window is furnished per feeder breaker, but breaker placement and depth of the rear cable compartment can allow the field of view of the IR window to cover multiple breaker terminations.


Figure 1.12: Infrared feeder stacks

## Remote racking

All EntelliGuard G breaker cassettes include provisions to accept a remote racking device that allows the operator or electrician to move the breaker anywhere between the DISCONNECT and CONNECT positions without standing in front of the circuit breaker cubicle. The remote racking device (Figure 1.13) attaches to the cassette without opening the cubicle door. It is powered from any standard 120 Vac receptacle. The control box (Figure 1.14) on the end of the 30 -foot cord has switches (power, breaker type, direction, and RUN) to control the operation of the remote racking device, allowing the operator to stand outside the arc flash boundary while racking a circuit breaker into or out of its cubicle.


Figure 1.13: Remote racking device


[^2]
## Cable space

The conduit entrance area (Figure 1.15) meets NEC requirements for cable termination and bending space. Extended depth frame options are available in 7 -in. or 14- in. sizes for applications requiring additional cable space. Breaker section widths can also be increased from 22 in . to 30 in . or from 30 in . to 38 in . for additional cable space.


Figure 1.15: Cable conduits

## Breaker lifting device

Installed on the top of the switchgear, this railmounted hoist provides the means for installing and removing EntelliGuard G breakers from the switchgear cubicles (Figure 1.16). The overhead breaker lifting device is standard on outdoorprotected aisle construction and optional on indoor construction. Alternatively, a hydraulic breaker lifter may be used to install and remove breakers. Lifting spreaders are provided as a standard accessory for each switchgear lineup. The breaker lifting spreader is the interface between the cable hook on the breaker lifting device and the circuit breaker. Lifting spreaders are also used with the hydraulic breaker lifter.


## Paint finish

The sheet metal parts that form the AKD-20 switchgear cubicles and sections are protected by a powder coat paint process, which utilizes polyester powder, electrostatically applied to properly prepared parts. Switchgear parts are moved through the process on a continuously moving overhead conveyor system.

A 10-stage surface preparation process includes:

- Two stages of cleaning - hot alkaline wash;
- Three stages of counter-flow rinsing;
- A phosphate treatment stage - heated iron phosphate coating;
- Rinse;
- Non-chrome sealer;
- Rinse;
- Final de-ionized water rinse.

The parts are dried in a separate oven and then travel to the Power Coat Room, where temperature and humidity are maintained within specific limits. Located in the Powder Coat Room is the Powder Coat Booth, where the sheet metal parts receive a coating of polyester powder, 2-3 mils thick. The polyester powder meets UL1332 and has a UL Yellow card certifying compliance with this UL specification.

The Powder Coat Booth includes manual spray guns that are used for reinforcement of recessed areas prior to the application of powder by automatic guns, ensuring that all parts are completely coated on all surfaces. Next, parts travel to the Cure Oven where the powder is flowed and cured to a hard, uniform finish.

The resulting ANSI-61 light gray paint finish far exceeds the requirements of UL1558 and ANSI C37.20.1, which require a minimum 200 hour salt spray test. Parts that have the powder coat applied per this process have passed 600 hours of neutral salt spray testing per ASTM B-117.

Other testing includes passing 1,000 hours in a humidity cabinet, cross hatch adhesion, impact and ductility tests. Meeting or exceeding the UL, ANSI, and ASTM requirements demonstrates that the paint finish on the AKD-20 switchgear enclosure will be able to provide long service in severe operating environments.

## Seismic certification

AKD-20 switchgear with EntelliGuard G circuit breakers has been shake-table tested in accordance with ICC-ES-AC156 to the requirements of IEEE-693-2005 and IBC-2015. AKD-20 switchgear has been certified for use in all IBC- 2015 Seismic Use Groups, Occupancy Importance Factors, and Seismic Design Categories, as well as qualified to IEEE- 693 for Moderate and High Seismic Loading conditions. Additionally, AKD-20 has been approved by the Office of Statewide Health Planning and Development (OSHPD) for applications in healthcare facilities.

## Outdoor options and features

Outdoor-protected aisle equipment comes standard with an overhead hoist (Figure 1.17). For outdoor non-walk-in equipment, an optional hydraulic breaker lift may be used.


[^3]For ease of breaker installation, outdoor protectedaisle equipment comes standard with double doors on the right side of the equipment aisle (as viewed facing front of the equipment). On longer lineups an additional door is provided on the left side of the equipment.

All aisle doors are padlock capable from the exterior and come standard with panic door latches on the interior (Figure 1.18). Consult the factory if additional doors or door location modifications are required.


Figure 1-18: Panic door


Figure 1.19: Handle with padlock (front view)


Figure 1.20: Handle with padlock (side angle)

All outdoor switchgear comes standard with hinged rear doors with built-in padlock provisions. For both front and rear doors, use a No. 3 Master padlock ( 0.281 in . diameter, 0.73 in . high closed [measured inside the lock shank]), or a No. 1 Master padlock ( 0.312 in . diameter shank, 0.92 in . high closed [measured inside the lock shank]) for locking the handle. (See Figure 1.19 and Figure 1.20.)

## EntelliGuard G Circuit breakers and trip units

## Circuit breaker standards and references

EntelliGuard G circuit breakers are the newest line of low voltage power circuit breakers (LVPCBs) evolved from the exceptional designs and practices of legacy breakers. EntelliGuard G breakers offer a truly global product platform that meets industry standards throughout the Americas, Europe and Asia (ANSI, UL, CSA, IEC, Lloyds Register of Shipping, etc.).

New, state-of-the-art EntelliGuard TU trip units enable breakers with advanced technology to provide system protection, local and remote monitoring, relaying, and communications. EntelliGuard TU trip units may be supplied with either Modbus or Profibus communications protocols. The breaker-trip unit system delivers superior circuit protection without compromising selectivity or arc flash protection.

The EntelliGuard system is yet another evolution of ABB core competencies in reliable electric power distribution, circuit protection, and arc flash protection. EntelliGuard G 3-pole breakers are the standard in ABB AKD- 20 low voltage switchgear.

The breakers are suitable for $240 \mathrm{Vac}, 480 \mathrm{Vac}$, and 600 Vac applications, and they provide advanced circuit protection, limit arc fault energy, and preserve system coordination without sacrificing any of these critical functions. Refer to Table 2.1 for applicable design and testing standards for EntelliGuard G breakers.

Table 2.1: Device standards and references

| ANSI certified low voltage power circuit breaker |
| :--- |
| C37.13 |
| C37.16 |
| C37.17 |
| C37.20.1 |
| UL1066 |

EntelliGuard G devices are available in all standard, $100 \%$ rated, ANSI, UL ratings in drawout designs (Table 2.2). All configurations can be manually or electrically operated with multiple and redundant accessories. Table 2.3 and Table 2.4 describe EntelliGuard G short circuit and interrupting ratings for automatic and non-automatic breakers.

Table 2.2: Device ratings, ANSI/UL1066 LVPCB

| Breaker size | Envelope 1 |  | Envelope 2 |  | Envelope 3 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type (see Table 2-3) | S | N/H/P | N | E/M | M | B/L |
| Available current sensors | 400 | 400 | - | 400 | - | - |
|  | 800 | 800 | - | 800 | - | - |
|  | 1200 | 1200 | - | - | - | - |
|  | - | 1600 | - | 1600 | - | - |
|  | - | 2000 | - | 2000 | - | - |
|  | - | - | 3200 | 3200 | - | 3200 |
|  | - | - | - | - | 4000 | 4000 |
|  | - | - | - | - | 5000 | 5000 |
|  | - | - | - | - | 6000 | 6000 |

Table 2.3: ANSI/UL1066 LVPCB interrupting ratings

| Interrupting rating tier ANSI/UL1066 devices, $\mathrm{I}_{\mathrm{cu}}$ |  |  |  | Breaker / Cassette size, continuous current range, close and latch rating |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 240 V | 480 V | 600 V |  | Envelope 1 |  |  | velope 2 |  | Envelope |  |
| Type | $\begin{array}{r} 240 \mathrm{~V} \\ \max \end{array}$ | $\begin{array}{r} 580 \mathrm{~V} \\ \max \end{array}$ | $\begin{array}{r} 630 \mathrm{~V} \\ \max \end{array}$ | (30-cycle) withstand, $\mathrm{I}_{\mathrm{cw}}$ | Cont. C curr. and L | Cont. curr. | $\begin{array}{r} \mathrm{C} \\ \text { and } \\ \mathrm{L} \\ \hline \end{array}$ | Cont. curr. | C and L | Cont. curr. | C and L |
| S | 65.000 | 65.000 | 50.000 | 50.000 | 400-1200 A | - | - | - | - | - | - |
| N | 65.000 | 65.000 | 65.000 | 65.000 | 400-2000 A | 3200 A | 65 | - | - | - | - |
| H | 85.000 | 85.000 | 65.000 | 65.000 | 400-2000 A | - | - | - | - | - | - |
| P | 100.000 | 100.000 | 65.000 | 65.000 | 400-2000 A | - | - | - | - | - | - |
| E | 85.000 | 85.000 | 85.000 | 85.000 | - | - | - | 400-3200 A |  | - | - |
| M | 100.000 | 100.000 | 100.000 | 85.000 | - | - | - | 400-3200 A |  | 4000-6000A |  |
| B | 100.000 | 100.000 | 100.000 | 100.000 | - | - | - | - | - | 3200-6000A | 100 |
| L | 150.000 | 150.000 | 100.000 | 100.000 | - | - | - | - | - | 3200-6000A |  |

Table 2.4: Non-automatic circuit breaker - ANSI version ratings

| Breaker <br> type | Amps | Rated interrupting <br> current (kA) | Minimum eechanical <br> endurance | Minimum electrical <br> endurance @480 V | Minimum electrical <br> endurance @600 V |
| :--- | ---: | ---: | ---: | ---: | ---: |
| S | 800 | 42 | 12.500 | 10.000 | 7.500 |
| N | 800 | 42 | 12.500 | 10.000 | 7.500 |
| N | 1600 | 42 | 12.500 | 10.000 | 7.500 |
| N | 2000 | 42 | 12.500 | 7.500 | 5.000 |
| M | 3200 | 65 | 5.000 | 5.000 | 5.000 |
| B | 4000 | 100 | 5.000 | 3.000 | 2.000 |
| B | 5000 |  | 5.000 | 2.000 | 1.500 |




## Standard and optional features

## Short time rating

Up to 100 kA for $1 / 2 \mathrm{sec}$. Types B and L.

## Short circuit/high interruption rating

150 kA at 600 V. Types B and L.

## Thermal performance

ANSI C37 designs are 100\% rated up to $40{ }^{\circ} \mathrm{C}$ when applied in recommended enclosure sizes.

## Reverse feed

EntelliGuard G devices can be fed from top or bottom terminals.

## Two-step stored energy mechanism

EntelliGuard G operates via stored energy mechanisms that can be manually charged (MO) or electrically charged (EO) by the Spring Charging Motor. Closing time is less than five cycles. Closing and opening can be initiated remotely or via the front cover pushbuttons. An Open-Close-Open cycle is possible without recharging. The breaker operating mechanism is a trip-free mechanism and is furnished with an integrated anti-pumping system.

Field-installable trip units and accessories Field-installable accessories are common to all breaker envelopes and frames.

## Coils (optional)

EntelliGuard G breakers have provisions for four accessory operating coils. The four positions can be filled as shown in Table 2.5. The Command Closing Coil (CCC) can accept a low-level signal (such as a PLC output) or a Modbus Command to close the breaker. Network Interlock is used to mechanically enable or block closing the circuit breaker by momentarily energizing the SET or RESET coils. Optional coil signaling contacts for the Shunt Trip, Close Coil, and UV accessory coils provide coil status (energized/de-energized) via the secondary disconnects and trip unit Modbus registers.

Table 2.5: Breaker accessory coil combinations

| Accessory coil position, left-to-right |  |  |  |
| :--- | :--- | :--- | :--- |
| 1 | 2 | 3 | 4 |
| Shunt Trip UV | CC/CCC | Shunt Trip \#2 |  |
| Shunt Trip UV | CC/CCC | UV \#2 |  |
| Network Interlock |  |  | CC/CCC |
| Shunt Trip, UV, CC, CCC are continuously rated |  |  |  |
| - Network Interlock coils are momentary rated |  |  |  |
| - CC/CCC include anti-pump function |  |  |  |
| - CCC includes electrical close PB on breaker escutcheon |  |  |  |
| - UV time delays: |  |  |  |
| - 50 msec, down to $50 \%$ sensed voltage |  |  |  |
| - 20 msec, less than $50 \%$ sensed voltage |  |  |  |
| - Up to 3 sec with separate Time Delay Module |  |  |  |

## Breaker/main contact status (standard)

 OPEN/CLOSED, ON/OFF indication is provided on the front cover.
## Motor operator (optional)

Heavy-duty motor/gearbox unit; easily accessible.

## Ready-to-close indicator (standard)

Provides visible indication of readiness for close operation.

Auxiliary switches (standard and optional)
Four designs available:

- Power rated (3NO+3NC) - standard;
- Power rated (3NO+3NC) + low signal (Hi-Fi) (2NO+2NC);
- Power rated ( $8 \mathrm{NO}+8 \mathrm{NC}$ );
- Power rated (4NO+4NC) + low signal (Hi-Fi) (4NO+4NC).

Table 2.6: Auxialiary switch ratings

| AC Ratings |  |  |
| :---: | :---: | :---: |
| AC | 220/240 V | 10 A |
|  | 110/120 V | 15 A |
| DC Ratings |  |  |
| DC | 240 V | 5 A (6 contacts in series) |
|  | 125 V | 10 A (3 contacts in series) |
|  | 24 V | 15 A |

## Interlocks (Standard)

Standard interlocks include:

- Drawout breaker: prevents the breaker from being closed unless it is in the TEST or CONNECT positions;
- Drawout breaker/Main contacts: prevents withdrawal/removal of the breaker unless the main contacts are OPEN. Access to the drawout mechanism racking screw is blocked when the breaker is CLOSED;
- Spring discharge interlock: Automatically discharges the closing springs when the breaker is moved from the DISCONNECT to the WITHDRAWN position. This prevents withdrawing a breaker from the cubicle with energy stored in the closing springs.


## Breaker status indicators (standard)

Standard indicators include:

- The breaker status indicator shows the condition of the main contacts as OPEN or CLOSED;
- The status of the closing springs is indicated as CHARGED or DISCHARGED;
- The draw-out position indicator on the cassette displays whether the breaker is in the CONNECT, TEST, or DISCONNECT position;
- The breaker also includes a switch that provides main contact status indication to the POWER LEADER ${ }^{\text {TM }}$ Power Management System;
- The optional Reduced Energy Let-Through (RELT) is provided with an ON/OFF contact closure to positively indicate whether or not the RELT function is active.


## Rejection feature (standard)

A factory-installed rejection feature prevents mismatching breakers and cassettes/ substructures to prevent:

- Inserting a breaker with a lower interrupting rating into a higher rated cassette/substructure;
- Inserting a higher current rated breaker into a lower rated cassette/substructure.


## Closed-door racking (standard)

The breaker racking mechanism is accessible through the front of the cassette and permits safely connecting and disconnecting the circuit breaker without opening the door and exposing personnel to live parts during the process.

## Padlocking devices (standard)

The padlocking device is standard on breakers and allows up to three padlocks with $1 / 4$ " to $3 / 8^{\prime \prime}$ diameter shanks to secure the breaker in the OPEN/TRIP FREE position. The front panel of the cassette/substructure permits locking the breaker drawout mechanism with up to three padlocks.

## Key interlock (optional)

Switchgear applications utilize a Kirk key interlock mounted in the cassette. A maximum of two key interlocks may fit in the cassette.

## Shutters (optional)

Shutters may be installed in any cassette.
Shutters are padlockable in the closed position.

## Carriage position switch (optional)

This optional cassette/substructure device permits local or remote indication of the circuit breaker drawout status (CONNECTED or TEST/ DISCONNECTED), 6NO/6NC singlepole, double-throw contacts are available.

## Lifting spreader (standard)

Furnished standard with all switchgear lineups. Used to attach lifting mechanism (hoist) cable to the breaker for insertion/removal.

## Mechanical counter (optional)

Provides a local record of the cumulative number of complete breaker closing operations.

## Bell alarm contact (optional)

Provided with a mechanical lockout feature, the bell alarm operates whenever the breaker trips due to a protective function (electrical fault).

## Racking handle (standard)

Furnished with each switchgear lineup. Moves the drawout breaker through the CONNECT, TEST, and DISCONNECT positions.

## EntelliGuard TU trip unit

For more detail on the EntelliGuard TU trip unit system on EntelliGuard G breakers, refer to publication DET-653, EntelliGuard G Circuit Breaker Application Guide.

## Introduction

The EntelliGuard TU trip unit offers optimum circuit protection and optimum system reliability simultaneously with little or no compromise to either of these critical functions. Reliability and arc flash protection, in one package, at the same time, all the time. EntelliGuard TU series trip units are available as the standard controller for new production EntelliGuard G ANSI/UL1066 circuit breakers.

## Reliability without compromising protection

Reliable protection of circuits and equipment has always been the circuit breaker's primary mission. Providing appropriate protection of the conductors, while preserving selective coordination, has been the primary focusof most system designers.

Modern economic reality, coupled with strict regulatory requirements, demand optimal system performance with increased sensitivity to the inherent power system hazards that face operating and maintenance personnel. Safety agencies, local authorities and owner-operators demand better personnel protection and state-of-the-art capabilities to minimize hazards while simultaneously preserving critical loads and system capabilities. These requirements often seem to be, and sometimes are, in conflict, pitting the speed and sensitivity required to improve arc flash protection against the delays and deliberate decision making required to maximize power system reliability. EntelliGuard TU, along with the EntelliGuard family of circuit breakers, offers flexible solutions for demanding circuit protection and circuit preservation environments. The EntelliGuard TU is designed to provide the utmost in system protection and reliability simultaneously, with little or no compromise.

## Arc flash and the EntelliGuard TU trip unit

Reducing arc flash hazards should be the primary concern when designing power systems. The EntelliGuard TU, especially in conjunction with the EntelliGuard G circuit breaker, provides significant flexibility towards solving arc flash hazard problems without excessive sacrifice of system reliability, in terms of selectivity. One way to lower potential incident energy is to ensure that circuit breakers are able to interrupt using their Instantaneous trips for all expected arcing faults.

The IEEE standard's calculations predict a wide range of possible arcing currents. The actual arcing currents may be lower or higher when consideration is given to the potential error in short circuit calculations, fault current data provided by the utility company, and variance in the actual arcing gap or enclosure's geometry where the arc occurs. Of particular concern should be the lower end of the possible range of current that may fall below the Instantaneous pickup of a circuit breaker or the current limiting threshold of a fuse. Dangerous incident energy may quickly increase when interruption time increases from a few cycles to a few seconds, even for low arcing current.

## Terminology

- $I_{n}$ : Trip plug rating in amperes. This is the current rating of the rating plug installed in the trip unit. This is the maximum Long Time pickup a trip unit can have with a specific plug installed. A sensor can usually be applied with plugs between $37.5 \%$ or $40 \%$ to $100 \%$ of the sensor rating. Plugs are labeled in amperes;
- $\mathbf{X}$ : X is a multiplier that may be applied in front of any rating value to denote a fraction of that rating. For example, the Long Time Pickup may be set at 0.5 X of In ;
- HSIOC: High Set Instantaneous Overcurrent, also known as the Override. This is an Instantaneous protection setting applied near the circuit breaker's withstand rating required to clear high magnitude faults quickly. In UL489 circuit breakers this is fixed; in UL1066 CBs the override may vary, if present at all;
- MCR: Making Current Release. A setting provided with each trip unit, based on the specific circuit breaker size, used to protect the circuit against closing on high magnitude faults. The MCR function immediately trips/opens the circuit breaker if high magnitude fault current is sensed at the instant the circuit breaker is closed;
- $I_{c w}$ : Short Circuit Withstand Rating of a particular circuit breaker in amperes. The withstand rating is defined differently within different standards, but it is always the value of current that a circuit breaker can withstand for some period of time without interrupting;
- $I_{c u}$ : Short Circuit Interrupting Rating (ISC), or ultimate interrupting rating (ICU) in IEC terms. The maximum shortcircuit interrupting rating of a circuit breaker in amperes.


## Long time protection

EntelliGuard TU offers two different shapes for Long Time protection curves. Each type of curve is available with 22 different time delays. The shapes may be described as circuit breaker-type characteristics and fuse-type characteristics. The nominal Long Time pickup is computed from the trip rating plug value (In) multiplied by the Long Time pickup setting. Long Time pickup setting multipliers are user adjustable, ranging from 0.5 to 1.0 in increments of 0.05 .

## Thermal long time overcurrent (circuit breaker-type characteristic)

The thermal $I^{2} t$ shape is similar to the typical curve of a thermal magnetic circuit breaker and matches the shape of many overcurrent devices used in industry today. The typical shape and range of settings may be seen in DES-090 (Figure 2.6).

## Fuse-shaped steep long time overcurrent

The steeper fuse characteristic is a straight line shape for application in systems where fuses and circuit breakers are used together. Twenty-two different time bands are available in each trip unit. Refer to DES-091 for timecurrent characteristics (Figure 2.7).

## Thermal memory

The Long Time and Short Time pickup algorithm also includes a cooling cycle that keeps track of current if it oscillates in and out of pickup range. This Thermal Memory is also active in case the circuit breaker trips on Long Time or Short Time to account for residual heating in conductors. If a circuit breaker is closed soon after a Long Time trip or Short Time trip, a subsequent trip may happen faster than indicated by the time current curve due to the residual cable Thermal Memory effect. In trips without control power, the Thermal Memory is powered from the Trip Unit battery. The cooling algorithm requires up to 14 minutes to fully reset to zero.

## Short time protection

## Short time pickup

EntelliGuard TU provides a wide range of Short Time pickup settings, I2t slope characteristics, and time bands to optimize selectivity while not unnecessarily sacrificing clearing time. Short Time pickup settings range from 1.5 to 12 times the Long Time pickup setting for the EntelliGuard G circuit breakers in Envelopes 1 and 2. The maximum Short Time pickup for Envelope 3 is 10.

## Short time bands

EntelliGuard TU comes with a wide range of adjustable Time Delay Bands, ranging from a minimum of 25 msec (clears in 80 msec ) to 417 msec (clears in 472 msec ). The bands are specially designed to pickup above various circuit breakers and trip systems to provide required selectivity while not sacrificing any more clearing time than required to provide the best possible arc flash protection. Refer to DES-092 for time-current characteristics (Figure 2.8).

## Short time $\mathrm{I}^{2} \mathrm{t}$ slopes

EntelliGuard Trip Unit offers three different Short Time $I^{2} t$ characteristics to allow optimized settings for selectivity and fast protection whenever possible. The position of the $I^{2} t$ slopes varies with the Long Time pickup of the respective circuit breaker. The intersection of the Short Time pickup and the Short Time delay band with the $I^{2} t$ slope varies with the Short Time pickup and time delay band.

## Ground fault protection

EntelliGuard TU trip unit offers the ultimate in Ground Fault protection. Each trip unit may be provided with the ability to accept a neutral sensor signal and generate an internal Zero Sequence phasor for Ground Fault protection. It may also be equipped with the ability to accept a Zero Sequence phasor signal from an external Zero Sequence CT or residual summation scheme using current transformers. Either Ground Fault method may be used to provide Ground Fault trip or Ground Fault alarm.

## Internal residual summation

EntelliGuard TU trip unit uses internal air core sensors for current sensing, and the signals are residually summed using advanced digital electronics. A neutral sensor may be located remotely and connected to the trip unit.

## External zero sequence input

EntelliGuard TU trip unit is able to accept input from an externally calculated Ground Fault current. The Ground Fault current may be derived using a single Zero Sequence CT or multiple phase CTs connected in a residual summation scheme. Applications for this capability include sensing at the ground return connection for a transformer or generator, as well application in multiple-source grounded systems.

## Ground fault pickup settings

All UL1066 circuit breakers are limited to a maximum nominal pickup setting of 1200 A per the National Electrical Code or 60\% of the sensor size, whichever is lower. The minimum setting is $20 \%$ of sensor size. Refer to DES-093 (Figure 2.9) for timecurrent characteristics.

## Instantaneous protection

EntelliGuard TU trip unit may provide several types of Instantaneous protection, depending on the circuit breaker in which it is installed.

The different types of Instantaneous protection are as follows:

- Adjustable Selective Instantaneous;
- Extended Range Adjustable Selective Instantaneous;
- High Set Instantaneous Overcurrent Trip;
- Making Current Release (MCR);
- Reduced Energy Let-Through Instantaneous Trip.

Each of these Instantaneous trips provides optimum protection, selectivity, or both as required for different applications. Refer to DES-094 for time-current characteristics
(Figure 2.10).

## Adjustable selective instantaneous

EntelliGuard TU uses an exclusive algorithm to recognize the wave shape of fault current within a cycle. With the improved analysis of the fault current wave shape, the trip unit allows the circuit breaker to trip immediately yet provide superior selectivity when used above current limiting circuit breakers or fuses. In many cases, the trip unit's Instantaneous pickup may be set quite low yet allow for complete selectivity up to the circuit breaker's full withstand level.

The Adjustable Selective Instantaneous will clear a fault in three cycles when used in 60 Hz or 50 Hz applications. Zone Selective Interlocking (ZSI) may be used with this Instantaneous function, allowing several breakers with overlapping Instantaneous protection to be selective with each other. Because each circuit breaker is set to trip instantaneously for faults within their respective zones of protection, fast protection and selectivity are achieved simultaneously.

EntelliGuard TU trip unit can be furnished with one of two Instantaneous adjustment ranges. The standard adjustable range may be as high as 15X the trip plug value. An optional Extended Range Adjustable Selective Instantaneous, as high as 30X, may be provided. LVPCBs allow for this adjustable Instantaneous trip to be turned off.

High set instantaneous overcurrent (HSIOC) EntelliGuard TU trip unit's HSIOC pickup is similar to the fixed override used by other trip units and circuit breakers in the industry. In EntelliGuard G, the HSIOC setting is changed automatically by the trip unit if the normal adjustable Instantaneous is turned off.

When the adjustable instantaneous setting is turned OFF, the HSIOC nominal setting becomes 98\% of the circuit breaker's Short Time Withstand rating, Square-rated breakers (breakers where the interrupting and Short Time Withstand ratings are the same) do not require the use of HSIOC.

## Making current release (MCR)

This form of Instantaneous protection is provided on all EntelliGuard G circuit breakers. The MCR provides very fast protection when the circuit breaker is closed and for the first six cycles thereafter. After the six cycles hove elapsed, the MCR is turned off and the circuit breaker reverts to its adjustable Instantaneous pickup and HSIOC, if provided. The MCR will pick up for currents exceeding 78\% of the breaker close and latch rating (see Table 2-3) and will clear the fault in 40 msec or less.

Reduced energy let-through (RELT) Instantaneous Trip EntelliGuard TU trip unit provides an optional second, useradjustable, RELT Instantaneous trip. This trip provides an alternate setting that temporarily gives the circuit breaker more sensitive pickup to provide better Instantaneous protection, only when better protection is needed and some selectivity may be sacrificed.

The RELT pickup is adjustable from 1.5X to 15 X of plug rating, independent of the normal adjustable selective Instantaneous. It may be set higher or lower than the selective Instantaneous. When EntelliGuard TU trip unit has the RELT Instantaneous pickup enabled, the trip unit provides a positive feedback signal via an optically isolated dry contact and serial communication.

This positive feedback indicates that the trip unit has received and processed the RELT input and the Instantaneous settings have been changed. EntelliGuard TU trip unit's RELT capability provides the ultimate in user flexibility for wiring and controlling an alternate Instantaneous setting for temporary use to reduce personnel hazard. The RELT Instantaneous pickup clears fault current in 42 msec or less at 60 Hz .

## Reduced energy let-through switch wiring

The RELT switch may be connected to a manually operated two-position switch, a remote sensor, or both simultaneously. The EntelliGuard TU trip unit provides positive feedback directly from the trip unit so that the user is able to verify that the signal was received by the trip unit and the settings have changed. A light may be connected to the source to indicate that control power is available to change the setting (Figure 2.4). When RELT is turned ON, the backlight on the trip unit display will flash. When the RELT input is removed to turn RELT OFF, the backlight will continue to flash for 15 seconds, allowing an operator to exit the arc flash boundary before the trip unit returns to its normal selective trip settings.


Figure 2.4: Integrated Switch and LED. Spring Return from TEST to OFF, maintained in $\mathrm{ON}^{\star}$

* This configuration provides positive indication that the trip unit has received and processed the RELT ON signal. It also provides a control power check.


Caution: It is recommended that RELT Output be wired to an appropriate annunciation when remote activation control of RELT is used.

## Zone selective interlocking (ZSI)

EntelliGuard TU trip unit's fast ZSI system is able to interlock Ground Fault, Short Time and Instantaneous. When the feeder's in-zone protection must be slowed to be selective with a branch protector, the main can be set faster than the feeder without a sacrifice in selectivity between the main and feeder.

Each circuit breaker in a ZSI scheme allows separate user settings for the restrained (backup) and unrestrained (in-zone protections) for Ground Fault and Short Time protection. Instantaneous protection may also be interlocked such that all circuit breakers above the one whose zone has the fault will shift from Instantaneous clearing to a 0.058 msec time band.

## Rating plugs

The EntelliGuard TU trip system is composed of trip units and trip rating plugs along with the sensors and wiring provided in the EntelliGuard G circuit breaker to support the trip. Rating plugs are used to lower the Long Time adjustment range of the sensor provided in the circuit breaker. The EntelliGuard TU trip rating plugs are unique in that they can be used with multiple trip units and circuit breakers within a specific sensor range, rather than with only a single specific sensor.

The trip rating plug catalog number, shown in Figure 2.5, identifies the rating as well as the minimum and maximum sensor rating the plug may be used with. Table 2.7 lists trip rating plugs available for each sensor. Table 2.8 lists the two-digit codes used within the trip rating plug catalog numbers and the sensor current ratings to which they are mapped.


Table 2.7: Trip rating plug specifications

| Trip plug <br> catalog <br> number | Plug rating | May be used with |  |
| :--- | ---: | ---: | ---: |

Table 2.8: Trip rating plug codes

| Sensor designation | Sensor rating |
| :--- | ---: |
| 04 | 400 A |
| 06 | 600 A |
| 07 | 630 A |
| 07 | 800 A |
| 10 | 1000 A |
| 12 | 1200 A |
| 13 | 1250 A |
| 16 | 1600 A |
| 20 | 2000 A |
| 25 | 2500 A |
| 30 | 3000 A |
| 32 | 3200 A |
| 40 | 4000 A |
| 50 | 5000 A |
| 60 | 6000 A |
| 64 | 6400 A |

## Universal spare trip unit

EntelliGuard G circuit breakers will accept a Universal Spare Trip Unit. This unique trip unit may be used in any EntelliGuard G circuit breaker regardless of frame size, sensor size, or short circuit rating. Should any circuit breaker's trip unit fail to operate for any reason, this one universal trip unit may be used as a replacement.

Once an EntelliGuard TU trip unit, including the Universal Spare Trip Unit, is associated with a specific EntelliGuard G circuit breaker, it may be used only with that specific circuit breaker. If exchange between EntelliGuard G circuit breakers is required, a trip unit may be interchanged only between circuit breakers with equal sensor ratings, short circuit ratings, and standard listing. Universal Trip Units may be ordered with a limited set of options. It is suggested that they be ordered with the widest range of options used within a facility, as any unnecessary functions can always be disabled or turned off (except for Ground Fault) during setup. Configurable options for the Universal Trip Unit are listed in Table 2.9.

## Protective relays

EntelliGuard TU offers various protective and alarm relay functions that may be displayed on the LCD screen, assigned contact outputs or communicated serially (Table 2.10).

Table 2.9: Universal Spare Trip Unit options (userselected)

| Feature | \# | Option |
| :---: | :---: | :---: |
| Long Time | 1 | Standard |
|  | 2 | Standard and fuse |
| Instantaneous | 1 | Standard |
|  | 2 | Extended range |
| Ground Fault* | 1 | None |
|  | 2 | Standard |
|  | 3 | Ground input |
| Arc Flash Protection | 1 | No RELT |
|  | 2 | RELT |
| Zone Selective Interlocking | 1 | Short Time and Ground fault |
|  | 2 | Short Time, Ground fault, and Instantaneous |
| Communications | 1 | None |
|  | 2 | Modbus |
|  | 3 | Profibus |
| Metering | 1 | Standard (ammeter) |
|  | 2 | Advanced (A, V, E and P) |
|  | 3 | Diagnostic (Advanced and WFC) |

* Mains and ties in solidly grounded multiple source substations will usually require ground input type Ground Fault Protection. Feeders will use standard internal ground fault protection.

Protective relays may be set by the user to alarm, trip the circuit breaker, or both. Alarms and trips are displayed on the local LCD trip and communicated serially. Alarms may also be assigned to one of two output contacts. The Trip and Alarm settings are independently set for each relay function.

## Trip logic inputs

The trip unit is able to receive two hardwired input signals (Table 2.10). Either can be a 24 Vac or Vdc signal. The inputs can be assigned to two main functionalities:

- Reduced Let Thru Energy (RELT)

Instantaneous protection "ON";

- Breaker "TRIP".

Table 2.10: Relay functions available in EntelliGuard G circuit breakers with EntelliGuard TU trip units

| Functions |  | Trip | Alarm | Display | Output contact ${ }^{(2)}$ | Serial comm. | Output ${ }^{(3)(4)}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | 1 | 2 | Dedicated |
| Protective | Voltage unbalance | Yes | Yes | Yes | Yes | Yes |  |  | - |
|  | Under voltage | Yes | Yes | Yes | Yes | Yes |  |  | - |
|  | Over voltage | Yes | Yes | Yes | Yes | Yes |  |  | - |
|  | Current unbalance | Yes | Yes | Yes | Yes | Yes |  |  | - |
|  | Power reversal | Yes | Yes | Yes | Yes | Yes |  |  | - |
| Status | Current level alarm, 2 settings available | No | Yes | Yes | Yes | Yes |  |  | - |
|  | Health indication (bad) | No | No | Yes | Yes | Yes |  |  | - |
|  | Health indication (good) | No | No | Yes | Yes | Yes |  |  | - |
|  | RELT ON Status3 | No | No | Yes | Yes | Yes |  |  | - |
|  | Ground fault alarm status | No | No | Yes | Yes | Yes |  |  | - |
|  | ZSI output | No | No | Yes | No | No | - | - |  |
| Diagnostics | Trip target | No | No | Yes | No | Yes | - | - | - |
|  | Trip information | No | No | Yes | No | Yes | - | - | - |
|  | Trip counter | No | No | Yes | No | Yes | - | - | - |
|  | Event logging (Trips, alarms, I/O) | No | No | Yes | No | Yes | - | - | - |
|  | Waveform Capture | No | No | No | No | Yes | - | - | - |
| Metering | Current (Phases A, B, C, N) | No | No | Yes | No | Yes | - | - | - |
|  | Voltage (Phase A, B, C) ${ }^{(1)}$ | No | No | Yes | No | Yes | - | - | - |
|  | Energy (kWh, Total) | No | No | Yes | No | Yes | - | - | - |
|  | Real power (watts, per phase and total) | No | No | Yes | No | Yes | - | - | - |
|  | Apparent power (VA, per phase and total) | No | No | Yes | No | Yes | - | - | - |
|  | Reactive power | No | No | Yes | No | Yes | - | - | - |

1. User set to PH-N or PH-PH.
2. Output contacts are low signal (Hi-Fi).
3. When trip unit has RELT, output 1 is dedicated to RELT ON status.
4. When breaker requires fans, output 2 is dedicated to the Fan control circuit.

## Outputs for EntelliGuard TU trip units

EntelliGuard TU trip units have two outputs, which are relay contact outputs to secondary disconnects. Each output can be configured per Table 2.11.

## Waveform capture

The Waveform Capture option in the advanced trip unit can track and visualize any fault event. The device tracks eight cycles, four before and four after the event, with resolution of 48 samples per cycle at 60 Hz , and stores the results in memory. It registers events in all three phases and the neutral.

After the event, the waveform is stored in COMTrade format and can be accessed by using the waveform client module of the Enervista software. (The PMCS system must be connected and running at the time of the event to capture waveform information.) When the upload into this software is complete, the trip unit will reset this function and be available to register the next event.

6000A AKD-20 and 5000A AKD-20 AR(Arc Res) breakers require the use of cooling fans to maintain temperatures within standards. The Relay output 2 is used to control an external contactor that switches power to the fan. Details of the automatic fan controls can be found in DEH-41472D or DEH-41304.

## EntelliGuard trip unit summary

Table 2.13 provides an overview of the trip unit features, characteristics, specifications, and accuracy.

Table 2.11: Input assignments possible

| Input | Assignment | Summary description |
| :--- | ---: | ---: |
|  | OFF | No action taken |
| 1 | TRIP | Will cause the circuit breaker to trip |
|  | RELT | Input causes the unit to use the RELT <br> set-point as long as input is active |
| 2 | OFF | No action taken |
|  | TRIP | Will cause the circuit breaker to trip |

Table 2.12: Output configuration

| Assignment | Summary description |
| :--- | ---: |
| GF alarm | Closes when GF alarm is activated. <br> Relay 1 or 2. |
| Overcurrent trip <br> (GF, INST, LT, ST) | Overcurrent trip closes the relay. <br> Relay 1 or 2. |
| RELT on | Closes relay when Reduced Let |
| Through Energy Instantaneous pickup |  |
| setting is enabled. Relay 1. |  |

Notice: Relay 1 may be used for the RELT function and not available for customer use. Relay 2 may be used when fans are required for a breaker and not available customer use.

Table 2.13: EntelliGuard trip unit summary

| Feature | Characteristic | Specification | Accuracy @ 100\% |
| :---: | :---: | :---: | :---: |
| Long time pickup and delays (standard) | CB curves | 22 (refer to Figure 2.6: DES-090) | - |
|  | Fuse-type curves | 22 (refer to Figure 2.7: DES-091) | - |
|  | Pickup range | 0.5-1.0 (.05 steps) x Rating Plug | - |
|  | CB Curve delay band range @6X | $0.5-22 \mathrm{sec}$ | - |
|  | Fuse-type curve delay band range @6X | 0.004-3.09 sec | - |
|  | Long time thermal memory | Switchable via Modbus | - |
| Short time pickup and delays (standard) | Pickup range | $1.5-12 \times$ LT Pickup (refer to Figure 2.8: DES-092 for max settings / breaker type) | - |
|  | ST delay band range (commit time) | $0.025 \mathrm{sec}-0.417 \mathrm{sec}$ and OFF | - |
|  | Band width | 55 msec | - |
|  | ST delay bands | 11 | - |
|  | $1^{2}$ t slopes | 3 | - |
| Instantaneous Protection (standard except as noted) | Adjustable pickup range | 2.0-15 x Rating Plug and OFF (refer to Figure 2.10: DES-094 for max settings / breaker type) | - |
|  | Extended range adjustable pickup | 2.0-30 x Rating Plug and OFF (refer to Figure 2.10: DES-094 for max settings / breaker type) - OPTIONAL | - |
|  | Making current release | 15 X instantaneous, first six cycles after closing | - |
|  | Override | Yes when ICW < ICU (30-cycle withstand is less than interrupting rating) | - |
|  | Alternate pickup with remote enable | Yes (RELT Instantaneous), 1.5-15 x Rating Plug - OPTIONAL | - |
|  | Selective instantaneous | Selective with current limiting MCCB, (selective with LVPCB and ICCB with unstantaneous ZSI) | - |
| Ground fault protection (optional) | Pickup range | 0.2-0.6 x Sensor, up to 1200 A pickup max (refer to Figure 2-9: DES-093) | - |
|  | External current sensor input | Yes, $63 \mathrm{~mA}=1$ per Unit | - |
|  | Delay band range | $0.047-0.91 \mathrm{sec}$ | - |
|  | Delay bands | 14 | - |
|  | $1^{2}$ t slopes | 2 | - |
|  | $1^{4}$ t slope | 1 | - |
|  | GF alarm option | Yes | - |
| Zone Selective Interlocking (Optional) | Short time and/or Ground fault | User selectable restrained and unrestrained time delays | - |
|  | Instantaneous | User selectable pickup | - |


| Feature | Characteristic | Specification | Accuracy @100\% |
| :---: | :---: | :---: | :---: |
| Protective relays (optional except as noted) | Current unbalance | 10-50\% difference between highest and lowest phase compared to average | $2 \%,+/-0.1 \mathrm{sec}$on delay |
|  |  | $1 \%$ steps, $1-15$ sec delay in 1 sec steps |  |
|  | Voltage unbalance | 10-50\% difference between highest and lowest phase compared to average | $\begin{array}{r} 2 \%,+/-0.1 \mathrm{sec} \\ \text { on delay } \end{array}$ |
|  |  | $1 \%$ steps, $1-15$ sec delay in 1 sec steps |  |
|  | Overvoltage | 110-150\% of sensed voltage | $2 \%,+/-0.1 \mathrm{sec}$ on delay |
|  |  | $1 \%$ steps, $1-15$ sec delay in 1 sec steps |  |
|  | Undervoltage | $50-90 \%$ of sensed voltage | $2 \%,+/-0.1 \mathrm{sec}$ on delay |
|  |  | $1 \%$ steps, $1-15$ sec delay in 1 sec steps |  |
|  | Power reversal | Line-to-Load or Load-to-Line | $2 \%$ |
|  |  | 10-990 kW in 10 kW steps |  |
|  | High current alarm - STANDARD | 2 | - |
|  |  | Independent pickup and drop-out settings for each alarm | - |
| Metering, diagnostics, and misc. functions (optional except as noted) | Current (A) | A, B, C-STANDARD | 0000 Resolution, 2\% |
|  | Voltage (V) | A-B, B-C, C-A or A-N, B-N, C-N (single phase values for line-to-neutral PT connection) | 0000 Resolution, 2\% |
|  | Real power (kW) | A, B, C, or Total (single phase values for line-toneutral PT connection) | 000.000 Resolution, 4\% |
|  | Reactive power (kVar) | A, B, C, or Total (single phase values for line-to-neutral PT connection) | 000.000 Resolution, 4\% |
|  | Apparent power (kVA) | A, B, C, or Total (single phase values for line-to-neutral PT connection) | 000.000 Resolution, 4\% |
|  | Energy (kWh) | Total | 000.000 Resolution, 4\% |
|  | Frequency (Hz) | Yes | 00 Resolution, 1 Hz |
|  | Real power demand (kW) | Total | 000.000 Resolution, 4\% |
|  | Power factor (\%) | A, B, C, or Total (single phase values for line-to-neutral PT connection) | 00 Resolution, 4\% |
|  | Peak power demand (kW) | Total | 000.000 Resolution, 4\% |
|  | Waveform capture | COMTrade file - requires PMCS | - |
|  | Trip operations counter | Yes-STANDARD | - |
|  | Event log | Last 10 events with Time and Date stamp - STANDARD | - |
| Serial communications (optional) | Open protocol | Modbus RTU, Profibus DP | - |
|  | Front port for local comm | Yes - Standard | - |
| I/O - STANDARD | Programmable relays | 2 Programmable Inputs, 2 Programmable Outputs | - |
| Flexibility | Universal rating plug | Yes | - |
|  | Universal spare trip unit | Yes | - |
|  | Interchangeable trip unit | Yes, breakers with equivalent ratings | - |

Figures 2.6 to 2.10 show EntelliGuard G time curves:

Figure 2.6: DES-090, long time circuit breaker characteristics


- Long-Time Pickup Range: 0.5X-1.0X Trip Rating Plug
- Curves apply at 60 Hz and from $-20^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}$ circuit breaker ambient temperature
- All Voltages: 600 Vac and below

Figure 2.7: DES-091, long time fuse-like characteristics


- Long-Time Pickup Range: 0.5X-1.0X Trip Rating Plug
- Curves apply at 60 Hz and from $-20^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}$ circuit breaker ambient temperature
- All Voltages: 600 Vac and below

Figure 2.8: DES-092A, short time pickup and delay bands


- Pickup range: $1.5 \mathrm{X}-12 \mathrm{X}$ Long Time pickup
- Curves apply at 60 Hz and from $-20^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}$ circuit breaker ambient temperature
- All Voltages: 600 Vac and below

Figure 2.9: DES-093A, ground fault characteristics


- Pickup range: $0.2 \times$ Sensor min.; $0.6 \times$ Sensor max.; not to exceed 1200 A
- Curves apply at 60 Hz and from $-20^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}$ circuit breaker ambient temperature. All Voltages: 600 Vac and below

Figure 2.10: DES-094A, instantaneous, override (HSIOC) and reduced energy let-through instantaneous (RELT)


- Pickup range: 2X-15X Trip Rating Plug standard; 2X-30X Trip Rating Plug extended range
- Maximum Pickup may be limited by CB AIC Rating or Withstand
- Curves apply at 60 Hz and from $-20^{\circ} \mathrm{C}$ to $55^{\circ} \mathrm{C}$ circuit breaker ambient temperature
- All Voltages: 600 Vac and below


## Accessories

A wide range of optional accessories are interchangeable across all EntelliGuard G power circuit breakers, regardless of nominal rating or envelope/frame size. As shown in Figure 2.11, each accessory incorporates easy-fit design features for quick installation.

-
Figure 2.11: Accessory mounting

## Motorized spring charging unit

The unique motor/gearbox unit is specially designed to operate with the full range of EntelliGuard G breakers. After a breaker close operation, the unit automatically recharges the spring and makes it ready for immediate reclose, should the need arise. High-speed recharging ensures that the springs are fully charged within approximately three seconds following a release. All electrically operated (EO) ANSI/UL breakers are equipped with "Spring Charged" contact for status indication. Available charge motor control voltages shown in Table 2.15.

Spring charge contact is power rated only, as shown in Table 2.14:

Table 2.14

| AC ratings |  | DC ratings |  |
| :--- | :--- | ---: | ---: |
| Voltage | Amps | Voltage | Amps |
| $110 \mathrm{~V}-130 \mathrm{~V}$ | $\mathrm{AC} 21^{1}-15 \mathrm{~A}$ | 24 V | $\mathrm{DC} 21^{1}-15 \mathrm{~A}$ |
|  | $\mathrm{AC} 23^{2}-10 \mathrm{~A}$ | $110-130 \mathrm{~V}$ | $\mathrm{DC} 21^{1}-10 \mathrm{~A}$ |
| $220 \mathrm{~V}-240 \mathrm{~V}$ | $\mathrm{AC} 21^{1}-10 \mathrm{~A}$ | 250 V | $\mathrm{DC} 21^{1}-5 \mathrm{~A}$ |
|  | $\mathrm{AC} 23^{2}-5 \mathrm{~A}$ | - |  |

1. Resistive loads.
2. Inductive loads

Table 2.15: Motor operators

| Envelope | Power consumption | Nominal control voltage | ANSI range | Cat no. |
| :---: | :---: | :---: | :---: | :---: |
| 1 | DC-300 W | $24 \mathrm{Vdc} / 30 \mathrm{Vdc}$ | - | GM0124DR |
|  |  | 48 Vdc | $38 \mathrm{~V}-56 \mathrm{~V}$ | GM01048DR |
|  |  | 60 Vdc | - | GM01060DR |
|  |  | 72 Vdc | - | GM01072DR |
|  |  | $110 \mathrm{Vdc} / 130 \mathrm{Vdc}$ | $100 \mathrm{~V}-140 \mathrm{~V}$ | GM0111ODR |
|  |  | 250 Vdc | $200 \mathrm{~V}-280 \mathrm{~V}$ | GM01250DR |
|  | AC-350 VA | 48 Vac | - | GM01048AR |
|  |  | 120 Vac | $104 \mathrm{~V}-127 \mathrm{~V}$ | GM01120AR |
|  |  | 240 Vac | 208 V-254V | GM01240AR |
|  |  | 277 Vac | - | GM01277AR |
| 2 and 3 | DC-480 W | $24 \mathrm{Vdc} / 30 \mathrm{Vdc}$ | - | GM0224DR |
|  |  | 48 Vdc | $38 \mathrm{~V}-56 \mathrm{~V}$ | GM02048DR |
|  |  | 60 Vdc | - | GM02060DR |
|  |  | 72 Vdc | - | GM02060DR |
|  |  | $110 \mathrm{Vdc} / 130 \mathrm{Vdc}$ | $100 \mathrm{~V}-140 \mathrm{~V}$ | GM02110DR |
|  |  | 250 Vdc | 200 V-280 V | GM02250DR |
|  | AC-560 VA | 48 Vac | - | GM02048AR |
|  |  | 120 Vac | $104 \mathrm{~V}-127 \mathrm{~V}$ | GM02120AR |
|  |  | 240 Vac | 208 V-254V | GM02240AR |
|  |  | 277 Vac | - | GM02277AR |

[^4]
## Circuit breaker closing coils - standard and command

Both closing coil options offer electrical remote release of the spring charged closing mechanism. Both options include a standard anti-pump safety feature ensuring that the close signal must be released before further close commands are allowed. The Command Close Coil additionally provides for local breaker electrical close and remote breaker close over communications via the EntelliGuard trip unit (Table 2.16).

Table 2.16: Closing Coil Characteristics

| Type | Power consumption | Nominal control voltage | Catalog number |
| :---: | :---: | :---: | :---: |
| Closing coil | DC: 350 W , 20 W (sealed) <br> AC: 350W (inrush), 20 W (sealed) | 24 Vdc | GCCNO24DR |
|  |  | $48 \mathrm{Vac} / \mathrm{dc}$ | GCCN048R |
|  |  | $60 \mathrm{Vdc}-72 \mathrm{Vdc}$ | GCCN060DR |
|  |  | $110 \mathrm{Vdc} /$ | GCCN120R |
|  |  | $130 \mathrm{Vdc} /$ |  |
|  |  | 120 Vac |  |
|  |  | 208 Vac | GCCN208AR |
|  |  | 220 Vdc/ | GCCN240R |
|  |  | 240 Vac |  |
|  |  | 250 Vdc/ | GCCN277R |
|  |  | 277 Vac |  |
| Command operated closing coil | DC: 350 W , 20 W (sealed) | 24 Vdc | GCCC024DR |
|  |  | $48 \mathrm{Vac} / \mathrm{dc}$ | GCCC048R |
|  |  | $60 \mathrm{Vdc}-72 \mathrm{Vdc}$ | GCCC060DR |
|  | $\begin{array}{r} \text { AC: 350W } \\ \text { (inrush), } \\ 20 \mathrm{~W} \text { (sealed) } \end{array}$ | $110 \mathrm{Vdc} /$ | GCCC120R |
|  |  | $130 \mathrm{Vdc} /$ |  |
|  |  | 120 Vac |  |
|  |  | 208 Vac | GCCC208AR |

- Duty cycle $=2 / \mathrm{min}$.
- Closing coil inrush $=350$ VA.


## Command operation module

This module energizes the closing coil to cause the breaker to close whenever commanded from the breaker trip unit or breaker front panel pushbutton (electrical closing). Remoteelectrical closing is also possible with the Command Close Coil.

## Shunt trip

Energizing the shunt trip (ST), via local or remote input, will instantaneously activate the circuit breaker mechanism, ensuring a rapid open operation (Table 2.17). The shunt trip is continuously rated and does not require an auxiliary switch in series with the coil.

Table 2.17: Extended range shunt trip for UL ground fault and ANSI DC rating applications

| Nominal control voltage | Catalog number |
| :--- | ---: |
| 24 Vdc | GSTG024DR |
| $48 \mathrm{Vac} / \mathrm{dc}$ | GSTG048R |
| $70 \mathrm{Vdc} / 72 \mathrm{Vdc}$ | GSTG072DR |
| $110 \mathrm{Vdc} / 125 \mathrm{Vdc} / 120 \mathrm{Vac}$ | GSTG120R |
| 208 Vac | GSTG208AR |
| 240 Vac | GSTG240R |
| $250 \mathrm{Vdc} / 277 \mathrm{Vac}$ | GSTG250R |

- Pickup range $=55 \%-110 \%$.
- Duty cycle = $2 / \mathrm{min}$.
- Inrush $=480 \mathrm{VA}(\mathrm{ac}), 480 \mathrm{~W}$ (dc).
- Holding $=60 \mathrm{VA}(\mathrm{ac}), 50 \mathrm{~W}(\mathrm{dc})$.


## Status indication switch (coil signaling contact)

A plug-in module is available to provide status indication via the secondary disconnects and trip unit. Coil signaling contacts are available for closing coils, shunt trips and under voltage releases (Table 2.18). The contact is mounted on top of the accessory device. One of the lowsignal (Hi-Fi) contacts is always wired to the trip unit.

Table 2.18: Coil-signaling contact module

| Type and configuration |  | Rating |  | Cat. no. |
| :---: | :---: | :---: | :---: | :---: |
| 1 power rated + <br> 1 low signal (Hi-Fi) (1NO contact each) | AC | 120 Vac | 6 A | GCSP1R |
|  |  | 250 Vac | 6 A |  |
|  |  | 125 Vac | 0.5 A |  |
|  | DC | 250 Vac | 0.25 A |  |
|  | AC | 125 Vac | 0.1 A |  |
|  | DC | 30 Vac | 0.1 A |  |
| 2 low signal (Hi-Fi) (1NO contact each) | AC | 125 Vac | 0.1 A | GCSP2R |

## Undervoltage release (UVR)

The UVR instantaneously activates the circuit breaker trip mechanism when the source voltage drops below the low voltage threshold (Table 2.19). The UVR is also a simple, field-installable device.

Notice: The undervoltage release acts as
$\square$ a permissive; It is a no voltage/no close device. The circuit breaker cannot be closed (manually or electrically) unless the UVR coil is energized above the required threshold.

Table 2.19: UVR operating characteristics

| Power <br> consumption | Nominal control <br> voltage | Catalog <br> number |
| :--- | ---: | ---: |
|  | 24 Vdc | GUVTO24DR |

- $20 \mathrm{msec}(1.2$ cycles) delay at $0 \mathrm{~V}, 50 \mathrm{msec}$ delay (3 cycles) at $50 \% \mathrm{~V}$
- Inrush = $350 \mathrm{VA}(\mathrm{ac}), 350 \mathrm{~W}$ (dc)
- Holding $=60$ VA (ac), 50 W (dc)


## Time delay module (TDM) for UVR

 (externally mounted)Operation of the Undervoltage Release can be delayed up to 3 seconds for applications where the breaker must be able to ride through momentary voltage interruptions. The Time Delay Module is mounted external to the circuit breaker and is connected between the voltage source and the breaker Undervoltage Release. Time delay is adjustable from 0 to 3 seconds. The time delay module starts its time delay at $50 \%$ of rated voltage (see Figure 2.12 and Table 2.19).


[^5]Table 2.20: TDM characteristics

| Nominal control voltage | Catalog no. |
| :--- | :--- |
| 48 Vdc | GTDM048D |
| 48 Vac | GTDM048A |
| 60 Vdc | GTDM060D |
| 125 Vdc | GTDM120D |
| 120 Vac | GTDM120A |
| 208 Vac | GTDM208A |
| 240 Vdc | GTDM240D |
| 240 Vdc | GTDM240A |
| 250 Vdc | GTDM250D |
| 277 Vac | GTDM277A |

## Ready-to-close contact

These contacts, as shown in Table 2.21, indicate that the following conditions are met and the circuit breaker can be closed:

- The circuit breaker is open;
- The closing springs are charged;
- The circuit breaker in not locked/ interlocked in the open position;
- There is no standing closing signal;
- There is no standing opening signal.

Table 2.21: Ready-to-close contacts (1 NO)

| Rating |  |  | Description | Catalog number |
| :---: | :---: | :---: | :---: | :---: |
| AC | 120 Vac | 6 A | high fidelity/ | GRTC2R |
|  | 250 Vac | 6 A | secondary disconnect | GRTC2R |
| DC | 125 Vac | 0.5 A | power rated/ secondary disconnect | GRTC1R |
|  | 250 Vac | 0.25 A | high fidelity/ trip unit | GRTC3R |

## Auxiliary switches

Auxiliary switches indicate breaker main contact position. They change their state in the same time sequence as the breaker main contacts. See Table 2.22 and Table 2.23 for available combinations and ratings.

Table 2.22: Auxiliary switches

| Nominal control voltage | Catalog no. |
| :--- | ---: |
| Power rated (3NO+3NC) | GAUX3R |
| Power rated (3NO+3NC) + low signal (Hi-Fi) <br> $(2 \mathrm{NO}+2 \mathrm{NC})$ | GAUX5R |
| Power rated (8NO+8NC) | GAUX6R |
| Power rated (4NO+4NC) + low signal (Hi-Fi) <br> $(4 \mathrm{NO}+4 \mathrm{NC})$ | GAUX8R |

Table 2.23: Auxiliary switch ratings and secondary disconnect points

| Contact <br> configuration | Power rated | Hi-Fi | Cat. no. |
| :--- | ---: | :---: | :---: |
| Power rated <br> (3NO+3NC) | A14-A25 | - | GAUX3R |
| Power rated | A14-A25 | B10-B13, | GAUX5R |
| (3NO+3NC) + |  | B23-B26 |  |
| low signal (Hi-Fi) |  |  |  |
| (2NO+2NC) |  |  |  |
| Power rated | A14-A25, |  | GAUX6R |
| (8NO+8NC) | B4-B13, |  |  |
|  | B17-B26 |  |  |
| Power rated | A14-A25, | B4-B11, | GAUX8R |
| (4NO+4NC) + | B12-B13, | B17-B24 |  |
| low signal (Hi-Fi) | B25-B26 |  |  |
| (4NO+4NC) |  |  |  |

- High Fidelity refers to gold-plated contacts. Use for signal level outputs ( 10 mA min. to 100 mA max., 8 Vdc to $30 \mathrm{Vdc}, 125 \mathrm{Vac}$ ).
- Power-rated contacts - $15 \mathrm{~A} / 440 \mathrm{~V}$.


## Key interlocks and door interlocks

EntelliGuard G breakers may be key-interlocked so that the breaker is held in a trip-free condition when the key is removed from the interlock. Key interlocks can be used on main and generator breakers or on main and tie breakers to prevent paralleling sources. Main circuit breakers may also be key-interlocked with transformer primary switches such that the secondary main breaker must be open before the primary switch can be operated. One or two key interlocks can be mounted in the cassette.

The key interlock also locks access to the racking mechanism when the breaker is locked open (Figure 2-13). Proper breaker position (CONNECT, TEST, or DISCONNECT) must be selected before engaging the key interlock.

An optional defeatable door interlock may also be incorporated into the cassette. This interlock is intended to prevent access to the breaker cubicle when the breaker is racked into the CONNECT position. The door interlock will latch the breaker cubicle door closed unless the breaker is racked out to the TEST or DISCONNECT position. If the breaker is in the CONNECT position and the door is closed, the door interlock can be manually overridden through a small hole in the breaker cubicle door. The door interlock does not trip the circuit breaker if the door is opened. Table 2.24 shows key and door interlock catalog numbers.


Figure 2.13: Cassette-mounted Key Interlock
Table 2.24: Key interlocks and door interlocks

| Description | Catalog no. |
| :--- | ---: |
| Mechanism for Kirk key cassette <br> interlock (cassette mounted) - key <br> interlock ordered separately | GCKRKR |
| Door interlock (left side) | GLHD |
| Kirk lock for cassette - extended | KCAMXXX10S* |
| Kirk lock for cassette - withdrawn | KCAMXXX11S* |

* S indicates that the key designation (A,B,etc.) is stamped on the
lock and key.


## Carriage position switch (TOC)

Available as an option and mounted on the side of the cassette/substructure, the carriage position switch provides six single-pole, double-throw (SPDT) contacts for local or remote electrical indication of the circuit breaker drawout status.

- GCPS2R provides two sets of contacts for each drawout breaker position: CONNECT - TEST DISCONNECT;
- GCPS3R provides six sets of contacts that change when the breaker is moved between the TEST and CONNECT positions.

See Table 2.25 for configurations and ratings.

Table 2.25: Carriage position switch configurations


[^6]
## Bell alarm with lockout

The Bell Alarm provides remote indication that the circuit breaker has opened because of an electrical fault. The Lockout feature is integral to the trip unit. In order to reclose the breaker after a fault, the Lockout button must be pushed in/reset on the trip unit (Table 2.26 and Table 2.27).

Table 2.26: Bell alarm switches

| Switch Configuration | Catalog no. |
| :--- | ---: |
| One single-pole, double-throw switch <br> (1-Form C contact) | GBAT1R |

Table 2.27: Bell alarm contact ratings

| Ratings |  |  |
| :--- | ---: | ---: |
| AC | 120 Vac | 6 A |
|  | 250 Vac | 6 A |
| DC | 125 Vdc | 0.5 A |
|  | 250 Vdc | 0.25 A |

## Charging spring status indicator

Factory-installed on the motor, this auxiliary switch indicates that the circuit breaker is charged (Table 2.28); it comes standard with the spring-charging motor.

Table 2.28: Spring-charged contact (1 NO)

| Ratings |  |  | Catalog number |
| :--- | ---: | ---: | ---: |
| AC | 120 Vac | 6 A |  |
|  | 250 Vac | 6 A |  |
| DC | 125 Vdc | 0.5 A | GSCC1R |
|  | 250 Vdc | 0.25 A |  |

## Secondary-disconnects (Factory-installed/ Field- installable)

Inputs and outputs to the circuit breaker are wired through secondary disconnects located on the top of the breaker. The plug-style secondary disconnects engage mating disconnects in the breaker cubicle when the breaker is in the TEST or CONNECT position. Up to 78 points are available so that all breaker accessories can be wired to a dedicated disconnect point (Table 2.29). Block B is ordered separately for cassettes, Cat. No. GSDWTR.

Table 2.29: Wiring schematic nomenclature definitionsand breaker wiring diagrams
\(\left.$$
\begin{array}{lrr}\hline \text { Ratings } & \text { Nomenclature } & \\
\hline \text { A1 } & \text { Motor } & \text { Motor } \\
\text { A2 } & \text { SPR NO/RTC NO } & \text { motor operator } \\
\hline \text { A3 } & \text { SPR NO/RTC NO } & \begin{array}{r}\text { spring charge status contact/ } \\
\text { A4 }\end{array}
$$ <br>

\hline ready to close signaling contact\end{array}\right]\)| power input to shunt trip 1 |
| :--- |
| A6 |


| Ratings Nomenclature |  |  |
| :---: | :---: | :---: |
| A24 | NO1 | normally open contact 1 |
| A25 | NO1 |  |
| A26 | - | - |
| A27 | O/P1a | relay output 1 from trip unit |
| A28 | O/P1b | relay output 1 from trip unit |
| A29 | O/P2a | relay output 2 from trip unit |
| A30 | O/P2b | relay output 2 from trip unit |
| A31 | $24 \mathrm{~V}+$ | auxiliary power supply |
| A32 | 24 V - | to trip unit |
| A33 | BA NC | bell alarm switch |
| A34 | BANO |  |
| A35 | BA COM |  |
| A36 | N-RC | neutral Rogowski coil |
| A37 | N-RC+ |  |
| A38 | Eleg-CT | earth leg CT (multi-source ground fault) |
| A39 | Eleg-CT |  |
| B1 | Input 1 | relay input to trip unit |
| B2 | Input 2 |  |
| B3 | I/P COMc |  |
| B4 | ST1 NO/NC8 | shunt trip 1 signaling contact/normally closed contact 8 |
| B5 | ST1 COM/NC8 |  |
| B6 | UV1 NO/NC7 | undervoltage release 1 signaling contact/normally closed contact 7 |
| B7 | UV1 COM/NC7 |  |
| B8 | NC6 | normally closed contact 6 |
| B9 | NC6 |  |
| B10 | NC5 | normally closed contact 5 |
| B11 | NC5 |  |
| B12 | NC4 | normally closed contact 4 |
| B13 | NC4 |  |
| B14 | - | - |
| B15 | - | - |
| B16 | - | - |
| B17 | CC NO/NO8 | closing coil signaling contact/normally open contact |
| B18 | CC COM/NO8 |  |
| B19 | ST2 NO/UV2 NO/NO7 | shunt trip 2 signaling contact/under voltage release 2 signaling contact/ |
| B20 | ST2 COM/UV2 COM/NO7 | normally open contact 7 |
| B21 | NO6 | normally open contact 6 |
| B22 | NO6 |  |
| B23 | NO5 | normally open contact 5 |
| B24 | NO5 |  |
| B25 | NO4 | normally open contact 4 |
| B26 | NO4 |  |
| B27 | ZSI out+ | GF zone selective interlock output |
| B28 | ZSI out- |  |
| B29 | ZSI in+ | GF zone selective interlock input |
| B30 | ZSI in- |  |
| B31 | ISO GND | trip unit communication |
| B32 | 5 V Iso | Modbus and Profibus |
| B33 | TX EN 1 |  |
| B34 | RX |  |
| B35 | TX |  |
| B36 | Voltage Input GND | - |
| B37 | Volt-A | system phase voltage signals |
| B38 | Volt-B |  |
| B39 | Volt-C |  |

Pages 46-49 show how to build an EntelliGuard catalog number based on available options.

Figure 2.14: Order guide: Catalog options


| Digit 5 | ort ci | it and | terrupting | g | mps) |  |  | Envelope 1 |  | Envelope 2 |  |  | Envelope 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 254 V | 508 V | 635 V | 30 Cycle Withstand | HSIOC | Override No INST | Override with INST | Code | $\begin{aligned} & 400 \text { A - } \\ & 1200 \text { A } \end{aligned}$ | $\begin{aligned} & 400 \mathrm{~A}- \\ & 2000 \mathrm{~A} \end{aligned}$ | $3200 \text { A }$ | $\begin{aligned} & 400 \mathrm{~A}- \\ & 3200 \mathrm{~A} \end{aligned}$ | $\text { A } 3200 \text { A }$ | $\begin{array}{r} 4000 \mathrm{~A}- \\ 6000 \mathrm{~A} \end{array}$ |
| 65000 | 65000 | 65000 | 50000 | 50000 | 49000 | 53500 | S |  | - | - |  | - - | - |
| 65000 | 65000 | 65000 | 65000 | - | - | - | N | - |  |  |  | - - | - |
| 85000 | 85000 | 85000 | 65000 | 65000 | 63700 | 69500 | H | - |  | - |  | - - | - |
| 100000 | 100000 | 100000 | 65000 | 65000 | 63700 | 69500 | P | - |  | - |  | - - | - |
| 85000 | 85000 | 85000 | 85000 | - | - | - | E | - | - | - |  | - | - |
| 100000 | 100000 | 100000 | 85000 | 85000 | 83800 | 90950 | M | - | - | - |  | - |  |
| 100000 | 100000 | 100000 | 100000 | - | - | - | B | - | - | - |  | - |  |
| 150000 | 150000 | 150000 | 100000 | 100000 | 98000 | 107000 | L | - | - | - |  | - |  |

1. Spring Charge Contact, GSCC1, supplied with all motor operators.
2. Electrically operated breakers require Closing Coil (Digit 8) and Shunt Trip Coil (Digit 9).
3. Both CC and CCC include anti-pump feature and manual close button.
4. CCC includes a local electrical close pushbutton on the breaker escutcheon.
5. Extended range shunt trip is required for external ground fault relaying applications.
6. Pickup range is $55-110 \%$ of the shunt trip coil voltage.
7. Fixed time delay, $50 \mathrm{msec} @ 50 \%$ Volts, $20 \mathrm{msec} @<50 \%$ Volts
8. External UVR time delay module available for $1-3$ sec delay.

Figure 2.14 (cont'd): Order guide: Catalog options


Figure 2.14 (cont'd): Order guide: Catalog options


- CCC - command operated close coil
- CSC - coil signaling contact
- Hi-Fi - High fidelity (low signal) gold-plated contact, 10 mA min, 100 mA max, $5-30 \mathrm{Vdc}, 125 \mathrm{Vac}$
- 3NO/3NC Aux switch contacts are wired to Sec Disc "A". All other aux switch options require Sec Disc "B"
- CSC via the TU requires a communications option on the TU (Digit 19)
- Non-automatic breakers cannot have CSC via the trip unit
- CSC selection is not valid if there are no accessory coils on the breaker (close, shunt trip, UV)

Figure 2.14 (cont'd): Order guide: Catalog options


Internal wiring diagram of EntelliGuard G breaker


AUXILIARY SWITCH CONTACTS
POWER RATED -- (CAN HAVE COIL SIGNALING CONTACTS) 3NO / 3NC -- A14-A25
POWER RATED -- (CANNOT HAVE COIL SIGNALING CONTACTS)
8NO / 8NC -- A14-A25, B4-B13, B17-B26
POWER RATED \& HIGH FIDELITY (SIGNAL RATED) -- (CAN HAVE COIL SIGNALING CONTACTS)
3NO / 3NC -- A14-A25 (POWER RATED)
2NO / 2NC -- B10-B13, B23-B26 (SIGNAL RATED)
POWER RATED \& HIGH FIDELITY (SIGNAL RATED) -- (CANNOT HAVE COIL SIGNALING CONTACTS) 4NO / 4NC -- A14-A25, B12-B13, B25-B26 (POWER RATED)
4NO / 4NC -- B4-B11, B17-B24 (SIGNAL RATED)

## Typical control circuit for EntelliGuard G breaker



[^7]
## Ground fault

EntelliGuard TU trip unit has provisions for two types of ground fault protection - internal sensing and external sensing. Internal ground fault sensing uses three-phase sensors plus a neutral sensor (Rogowski coil - see Table 2.30) for summation of the phase and neutral currents. If the summation of the phase and neutral currents exceeds the trip unit ground fault pickup and delay settings, the breaker will trip or the trip unit can provide a ground fault alarm. Internal ground fault sensing is typically applied to feeder breakers (3-wire or 4-wire) and to main breakers (3-wire only).

External ground fault sensing uses a single current sensor input as the ground fault signal. All summations of currents are performed external to the trip unit. Examples of external ground fault sensing are multisource ground fault on 4-wire systems and ground-return sensing. External ground fault sensing pickup settings are based on the rating of the phase sensors on the breaker.

The input from the external current sensors must be scaled such that 63 mA corresponds to 1 per unit of current.For example, the external current sensor used with a 4000 A breaker would be scaled so that 63 mA from the external current sensor would equal 4000 A .

The external ground fault sensors ( 5 amp relayclass current transformers) must have a primary rating that matches the phase sensor rating on the breaker. A summing and auxiliary CT sums and scales the secondary current from the ground fault sensors before providing the ground fault signal to the trip unit. Table 2.31 lists the summing and auxiliary CTs for external ground fault sensing. A more detailed description of external ground fault applied to multiple-source systems (double-ended substations) is provided in pages 55-77.

Table 2.30: Neutral Rogowski CTs (encased with terminal screws)

| Envelope | Current rating | Cat. no. |
| :---: | :---: | :---: |
| 1 | 400 A | G04HNRCE |
|  | 800 A | G08HNRCE |
|  | 1200 A/1500 A | G13HNRCE |
|  | 1600 A | G16HNRCE |
|  | 2000 A | G20HNRCE |
| 2 | 400 A | G04MNRCE |
|  | 800 A | G08MNRCE |
|  | 1600 A | G16MNRCE |
|  | 2000 A | G20MNRCE |
|  | 3200 A | G32HNRCE |
| 3 | $3000 \mathrm{~A} / 3200 \mathrm{~A}(1600 \mathrm{~A} \times 2)$ | G32LNRCE |
|  | 4000 A (2000 A $\times 2$ ) | G32LNRCE |
|  | $5000 \mathrm{~A}(2500 \mathrm{~A} \times 2)$ | G50LNRCE |

Table 2.31: EntelliGuard G summing and auxiliary CT

| Summing/Aux. CT <br> catalog number <br> 0173B4934__-_ | Ground fault <br> CT ratio | Summing CT <br> input | Summing CT <br> output | Summing CT <br> turns ratio | Auxiliary CT <br> ratio |
| :--- | ---: | ---: | ---: | ---: | ---: |
| P002 | $1200: 5$ |  | 0.1515 A | $132: 1$ | $0.60: 1$ |
| P003 | $1600: 5$ |  | 0.2000 A | $100: 1$ | $0.79: 1$ |
| P004 | $2000: 5$ |  | 0.2500 A | $80: 1$ | $0.99: 1$ |
| P007 | $3200: 5$ | $5+5+5+5$ |  | 0.4167 A | $48: 1$ |
| P008 | $4000: 5$ |  | 0.5000 A | $40: 1$ | $1.65: 1$ |
| P009 | $5000: 5$ |  | 0.6250 A | $32: 1$ | $1.98: 1$ |
| P010 | $6000: 5$ |  | 1.0 A | $20: 1$ | $2.47: 1$ |

## Mechanical operations counter

Used with either manual or motor charged circuit breakers, the counter provides an accurate record of the cumulative number of complete breaker closing operations (Table 2.32).

Table 2.32: Operations counter

| Description | Cat.no. |
| :--- | :---: |
| Mechanical operations counter | GMCNR |

Table 2.33: Wiring schematic for block-a (three layer secondary disconnect with basic GTU and basic accessories)

|  | A1 | A2 | A3 | A4 | A5 | A6 | A7 | A8 | A9 | A10 | A11 | A12 | A13 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Spr NO/ Spr NO/ |  |  |  |  |  |  |  |  | CC | CC | ST2/ | ST2/ |
|  | Motor | Motor | RTC NO | RTC NO | ST1 | ST1 | UV1 | UV1 | CC COM | IMM | CMD | UV2 | UV2 |
| Max. current (I) | 14.8A | 14.8A | 10A | 10A | 1.9A | 1.9A | 1.9A | 1.9A | 1.9A | 1.9A | 1.9A | 1.9A | 1.9A |
| Max. <br> voltage (V) | 440V | 440V | 240 V | 240 V | 440 V | 440 V | 440V | 440V | 440V | 440V | 440V | 440 V | 440 V |
|  | A14 | A15 | A16 | A17 | A18 | A19 | A20 | A21 | A22 | A23 | A24 | A25 | A26 |
|  | NC3 | NC3 | NC2 | NC2 | NC1 | NC1 | NO3 | NO3 | NO2 | NO2 | NO1 | NO1 |  |
| Max. current (I) | 15A | 15A | 15A | 15A | 15A | 15A | 15A | 15A | 15A | 15A | 1A | 15A |  |
| Max. voltage (V) | 440V | 440V | 440V | 440V | 440V | 440V | 440V | 440V | 440 V | 440V | 440V | 440 V |  |
|  | A27 | A28 | A29 | A30 | A31 | A32 | A33 | A34 | A35 | A36 | A37 | A38 | A39 |
|  | O/P1a | O/P1b | O/P2a | O/P2b | $24 \mathrm{~V}+$ | 24V- | BA NC | BA NO | BA COM | N-RC- | N-RC+ | Eleg-CT | Eleg-CT |
| $\begin{aligned} & \text { Max. } \\ & \text { current (I) } \end{aligned}$ | 1A | 1A | 1A | 1A | $\begin{array}{r} <500 \\ \mathrm{~mA} \end{array}$ | $\begin{array}{r} <500 \\ \mathrm{~mA} \end{array}$ | 10A | 10A | 10A | $\begin{aligned} & <50 \\ & m A \end{aligned}$ | $\begin{aligned} & <50 \\ & m A \end{aligned}$ | 5A | 5A |
| Max. voltage (V) | 30Vdc/ <br> 25 Vac | 30Vdc/ <br> 25 Vac | $\begin{array}{r} 30 \mathrm{Vdc} / \\ 25 \mathrm{Vac} \\ \hline \end{array}$ | 30Vdc/ 25 Vac | 30 V | 30V | 240 V | 240 V | 240V | 480mV | 480mV | 2V | 2V |

Table 2.34: Wiring schematic for block-b (three layer secondary disconnect to be added for GTU with full I/O and additional accessory ignals)

|  | B1 | B2 | B3 | B4 | B5 | B6 | B7 | B8 | B9 | B10 | B11 | B12 | B13 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INPUT1 | INPUT2 | I/P COM | ST1 NO/ <br> NC8 | $\begin{array}{r} \text { ST1 } \\ \text { COM/ } \\ \text { NC8 } \end{array}$ | UV1 NO/ NC7 | $\begin{array}{r} \text { UV1 } \\ \text { COM/ } \\ \text { NC7 } \end{array}$ | NC6 | NC6 | NC5 | NC5 | NC4 | NC4 |
| Max. <br> current (I) | <50mA | <50mA | <50mA | $\begin{array}{r} \hline 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | $\begin{array}{r} \hline 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | $\begin{array}{r} \hline 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | $\begin{array}{r} \hline 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | 15A | 15A | 15A | 15A | 15A | 15A |
| Max. <br> voltage (V) | 30Vdc/ 25 Vac | 30Vdc/ 25 Vac | 30Vdc/ 25 Vac | $\begin{gathered} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{gathered}$ | $\begin{gathered} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{gathered}$ | $\begin{gathered} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{gathered}$ | $\begin{gathered} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{gathered}$ | 440 V | 440 V | 440 V | 440 V | 440 V | 440 V |
|  | B14 | B15 | B16 | B17 | B18 | B19 | B20 | B21 | B22 | B23 | B24 | B25 | B26 |
|  | - | - |  | $\begin{array}{r} \hline \text { CC NO/ } \\ \text { NO8 } \end{array}$ |  | ST2 <br> NO/ <br> UV2 <br> NO/ <br> NO7 | $\begin{array}{r} \text { ST2 } \\ \text { COM/ } \\ \text { UV2 } \\ \text { COM/ } \\ \text { NO7 } \end{array}$ | NO6 | NO6 | NO5 | NO5 | NO4 | NO4 |
| Max. <br> current (I) | <50mA | < 500 mA |  | $\begin{array}{r} 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | $\begin{array}{r} 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | $\begin{array}{r} 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | $\begin{array}{r} 10 \mathrm{~A} / \\ 15 \mathrm{~A} \end{array}$ | 15A | 15A | 15A | 15A | 15A | 15A |
| Max. <br> voltage (V) | 5V | 0.1 V | - | $\begin{array}{r} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{array}$ | $\begin{gathered} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{gathered}$ | $\begin{array}{r} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{array}$ | $\begin{gathered} 240 \mathrm{~V} / \\ 440 \mathrm{~V} \end{gathered}$ | 440 V | 440V | 440V | 440 V | 440 V | 440 V |
|  | B27 | B28 | B29 | B30 | B31 | B32 | B33 | B34 | B35 | B36 | B37 | B38 | B39 |
|  | ZSI out+ | $\begin{gathered} \text { ZSI } \\ \text { out- } \end{gathered}$ | ZSI in+ | ZSI in- | $\begin{aligned} & \text { ISO } \\ & \text { GND } \end{aligned}$ | $\begin{array}{r} 5 \mathrm{~V} \\ \text { ISO } \end{array}$ | TXEN 1 | RX | TX | GND Volt-IN | Volt-A | Volt-B | Volt-C |
| Max. <br> current (I) | <50mA | <50mA | <50mA | < 50 mA | $\begin{array}{r} <500 \\ \mathrm{~mA} \end{array}$ | $\begin{array}{r} <500 \\ \mathrm{~mA} \end{array}$ | < 50 mA | < 50 mA | <50mA | $\begin{array}{r} <500 \\ \mathrm{~mA} \end{array}$ | <50mA | < 50 mA | < 50 mA |
| Max. voltage (V) | 28 Vdc | 28 Vdc | 30 Vdc | 30 Vdc | 0.1 V | 5 V | 5 V | 5 V | 5 V | 0.1 V | 1.76 V | 1.76 V | 1.76 V |

Table 2.35: Electronic interlock

| Network interlock connections |  |  | Network interlock status switch |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| A5 | A6 | A5 | A8 | B4 | B5 | B6 |
| NI TRIP | NI TRIP | NI RESET | NI RESET | NI NC | NI NO | NI COM |
| 1.9 A | 1.9 A | 1.9 A | 1.9 A | 10 A | 10 A | 10 A |
| 240 V | 240 V | 240 V | 240 V | 240 V | 240 V | 240 V |

## Application data

## EntelliGuard G power circuit breaker selection tables

The tables on the following pages can be used to help determine the correct EntelliGuard G breaker frame sizes and interrupting ratings based on the system voltage, transformer kVA rating, transformer overload ratings, and transformer impedance. The tables also provide arc flash incident energy values at the feeder sections based on the noted assumptions and the calculation methods provided in IEEE 1584. Main breakers are sized based on either the transformer base kVA or the transformer full load current with fan cooling. The main breaker short circuit rating is based on the transformer base kVA rating, minimum transformer impedance, and the system voltage.

Recommended feeder breakers are listed in two columns. Feeder breaker short circuit rating is determined by the combined short circuit current available from the transformer and any contribution from connected motor loads.

The first feeder breaker column provides the breaker designation based on the required short circuit interrupting rating. The breaker in this column has a short time withstand rating less than or equal to the breaker interrupting rating. The second feeder breaker column lists the feeder circuit breaker with a short time withstand rating equal to its interrupting rating or a "square-rated" breaker. The EntelliGuard G circuit breaker application guide discusses breaker short time withstand versus interrupting ratings and the use of the various instantaneous trip functions to achieve the required interrupting ratings while maintaining selectivity. To determine the transformer full load current based on the transformer type, kVA, temperature rise, andfan cooling, see Table 3.1.

Table 3.1: Transformer full-load current

| Transformer type | Self-cooled kVA | Percent increase <br> with fans |
| :--- | ---: | ---: |
| Liquid filled | $750-2000$ | $15 \%$ |
| $65^{\circ} \mathrm{C}$ rise | $2500-5000$ | $25 \%$ |
|  | $750-2000$ | $15 \%($ fans $)$ <br> $+12 \%\left(65^{\circ} \mathrm{C}\right)$ |
| Liquid filled | $2500-5000$ | $25 \%($ fans $)$ <br> $+12 \%\left(65{ }^{\circ} \mathrm{C}\right)$ |
| $5^{\circ} \mathrm{C} / 65^{\circ} \mathrm{C}$ rise | $750-2500$ | $33 \%$ |
| Ventilated dry | $500-2500$ | $40 \%$ |
| Cast coil | $3000-5000$ | $25 \%$ |

Table 3.2 shows the first five characters in the breaker catalog number, which define the breaker current and interrupting rating. These breaker designations are used in the following breaker selection tables.

Table 3.2: Breaker catalog number description for breaker selection table ${ }^{(1)}$

| ACB family |  |  | Code |
| :---: | :---: | :---: | :---: |
| EntelliGuard G |  |  | G |
| ANSI/UL1066 (breaker/vassette Size) |  |  | Code |
| Envelope 1 |  |  | N |
| Envelopes 2 and 3 |  |  | A |
| Current Rating <br> (Max Sensor) | Code | Breaker/ Cassette Size | AIC Rating Code ${ }^{(2)}$ |
| 800 A | 08 | 1 | S/N/H/P |
|  |  | 2 | E/M |
| 1200 A | 12 | 1 | S |
| 1600 A | 16 | 1 | N/H/P |
|  |  | 2 | E/M |
| 2000 A | 20 | 1 | N/H/P |
|  |  | 2 | E/M |
| 3200 A | 32 | 2 | E/M |
|  |  | 3 | B/L |
| 4000 A | 40 | 3 | M/B/L |
| 5000 A | 50 | 3 | M/B/L |
| 64000 A | 60 | 3 | M/B/L |

[^8]Table 3.3: System voltage @600 V - Nominal transformer Z (\%) = $5.75 \pm 7.5 \%$; Minimum transformer $\mathbf{Z}$ (\%) = 5.32
Voltage Rating: 600 V

| Transformer KVA | Full load current <br> (A) | Primary short circuit ${ }^{4}$ (MVA) | $\begin{gathered} \text { System } \\ \text { Z (\%) } \\ \hline \end{gathered}$ | Available SC curr. (A), nom. $Z$ | Available SC curr. $\text { (A), } \min Z$ | Motor contribution, 100\% motor load (A) | Max. combined fault curr. <br> (A) | $\begin{array}{r} \text { Arc flash } \\ \text { incident } \\ \text { energy }{ }^{(6)(7)} \\ (\mathrm{cal} / \mathrm{cm} 2) \end{array}$ | Mainbreaker <br> (1)(2)(3) <br> $I_{c w}>I_{s c}$ |  | Feeder breaker ${ }^{(5)}$ $\begin{array}{r} \mathrm{I}_{\mathrm{cw}}=\mathrm{I}_{\mathrm{cu}} \text { or } \\ \mathrm{I}_{\mathrm{cw}}>\mathrm{I}_{\mathrm{sc}} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 500 | 481 <br> with <br> fans: <br> 674 | 50 | 1.00 | 7128 | 7614 | 1925 | 9539 | 1.47 | GA08E <br> (GA08E) | GN08S | GN08N |
|  |  | 100 | 0.50 | 7698 | 8269 |  | 10193 | 1.57 |  |  |  |
|  |  | 150 | 0.33 | 7909 | 8512 |  | 10437 | 1.60 |  |  |  |
|  |  | 250 | 0.20 | 8086 | 8086 |  | 10643 | 1.63 |  |  |  |
|  |  | 500 | 0.10 | 8224 | 8879 |  | 10803 | 1.66 |  |  |  |
|  |  | 750 | 0.07 | 8271 | 8934 |  | 10858 | 1.67 |  |  |  |
|  |  | Unlimited | 0.00 | 8367 | 9046 |  | 10970 | 1.68 |  |  |  |
| 750 | $\begin{array}{r} 722 \\ \text { with fans: } \\ 1010 \end{array}$ | 50 | 1.50 | 9954 | 10584 | 2887 | 13471 | 2.05 | GA08E <br> (GA16E) | GN08S | GN08N |
|  |  | 100 | 0.75 | 11103 | 11892 |  | 14779 | 2.25 |  |  |  |
|  |  | 150 | 0.50 | 11547 | 12403 |  | 15290 | 2.32 |  |  |  |
|  |  | 250 | 0.30 | 11929 | 12844 |  | 15731 | 2.39 |  |  |  |
|  |  | 500 | 0.15 | 12232 | 13197 |  | 16083 | 2.44 |  |  |  |
|  |  | 750 | 0.10 | 12337 | 13318 |  | 16205 | 2.46 |  |  |  |
|  |  | Unlimited | 0.00 | 12551 | 13569 |  | 16456 | 2.50 |  |  |  |
| 1000 | $962$ <br> with fans: $1347$ | 50 | 2.00 | 12416 | 13148 | 3849 | 16997 | 2.58 | GA16E <br> (GA16E) | GN08S | GN08N |
|  |  | 100 | 1.00 | 14256 | 15228 |  | 19077 | 2.88 |  |  |  |
|  |  | 150 | 0.67 | 14996 | 16077 |  | 19926 | 3.01 |  |  |  |
|  |  | 250 | 0.40 | 15646 | 16826 |  | 20675 | 3.12 |  |  |  |
|  |  | 500 | 0.20 | 16172 | 17436 |  | 21285 | 3.21 |  |  |  |
|  |  | 750 | 0.13 | 16356 | 17649 |  | 21498 | 3.24 |  |  |  |
|  |  | Unlimited | 0.00 | 16735 | 18092 |  | 21941 | 3.30 |  |  |  |
| 1500 | with fans:$2021$ | 50 | 3.00 | 16496 | 17351 | 5774 | 23124 | 3.48 | $\begin{gathered} \text { GA16E } \\ (\text { GA20E }) \end{gathered}$ | GN08S | GN08N |
|  |  | 100 | 1.50 | 19909 | 21168 |  | 26941 | 4.03 |  |  |  |
|  |  | 150 | 1.00 | 21383 | 22843 |  | 28616 | 4.28 |  |  |  |
|  |  | 250 | 0.60 | 22730 | 24386 |  | 30160 | 4.50 |  |  |  |
|  |  | 500 | 0.30 | 23857 | 25689 |  | 31462 | 4.69 |  |  |  |
|  |  | 750 | 0.20 | 24258 | 26154 |  | 31928 | 4.76 |  |  |  |
|  |  | Unlimited | 0.00 | 25102 | 27137 |  | 32911 | 4.76 |  |  |  |
| 2000 | $\begin{array}{r} 1925 \\ \text { with fans: } \\ 2694 \end{array}$ | 50 | 4.00 | 19738 | 20652 | 7698 | 28350 | 4.24 | $\begin{array}{r} \text { GA20E } \\ (\text { GA32N }) \end{array}$ | GN08S | GN08N |
|  |  | 100 | 2.00 | 24832 | 26295 |  | 33993 | 5.06 |  |  |  |
|  |  | 150 | 1.33 | 27169 | 28931 |  | 36629 | 5.44 |  |  |  |
|  |  | 250 | 0.80 | 29382 | 31453 |  | 39151 | 5.80 |  |  |  |
|  |  | 500 | 0.40 | 31293 | 33652 |  | 41350 | 6.12 |  |  |  |
|  |  | 750 | 0.27 | 31986 | 34456 |  | 42154 | 6.23 |  |  |  |
|  |  | Unlimited | 0.00 | 33470 | 36183 |  | 43881 | 6.48 |  |  |  |


| Transformer KVA | Full load current <br> (A) | Primary short circuit ${ }^{4}$ (MVA) | $\begin{array}{r} \text { System } \\ \text { Z (\%) } \end{array}$ | Available SC curr. <br> (A), nom. $Z$ | Available SC curr. (A), min Z | Motor contribution, 100\% motor load (A) | Max. combined fault curr. <br> (A) | $\begin{array}{r} \text { Arc flash } \\ \text { incident } \\ \text { energy } \\ \left({ }^{(6)(7)} 7\right. \\ \text { (cal/cm2) } \end{array}$ | Main breaker (1)(2)(3) $\mathrm{I}_{\mathrm{cw}}>\mathrm{I}_{\mathrm{sc}}$ | $\begin{array}{r} \text { Feeder } \\ \text { breaker }{ }^{(5)} \\ \mathrm{I}_{\mathrm{cw}} \leq \mathrm{I}_{\mathrm{cu}} \end{array}$ | Feeder breaker ${ }^{(5)}$ $\begin{array}{r} \mathrm{I}_{\mathrm{cw}}=\mathrm{I}_{\mathrm{cu}} \text { or } \\ \mathrm{I}_{\mathrm{cw}}>\mathrm{I}_{\mathrm{sc}} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2500 | $\begin{array}{r} 2406 \\ \text { with fans: } \\ 3368 \end{array}$ | 50 | 5.00 | 22378 | 23313 | 9623 | 32936 | 4.90 | $\begin{array}{r} \text { GA32N } \\ \text { (GA40M) } \end{array}$ | GN08N | GN08N |
|  |  | 100 | 2.50 | 29159 | 30767 |  | 40390 | 5.98 |  |  |  |
|  |  | 150 | 1.67 | 32435 | 34438 |  | 44060 | 6.51 |  |  |  |
|  |  | 250 | 1.00 | 35639 | 38071 |  | 47694 | 7.03 |  |  |  |
|  |  | 500 | 0.50 | 38490 | 41343 |  | 50965 | 7.50 |  |  |  |
|  |  | 750 | 0.33 | 39545 | 42562 |  | 52184 | 7.67 |  |  |  |
|  |  | Unlimited | 0.00 | 41837 | 45229 |  | 54852 | 8.05 |  |  |  |
| 3000 | $\begin{array}{r} 2887 \\ \text { with fans: } \\ 4041 \end{array}$ | 50 | 6.00 | 24568 | 25504 | 11547 | 37051 | 5.50 | $\begin{array}{r} \text { GA32N } \\ \text { (GA50M) } \end{array}$ | GA08E | GA08E |
|  |  | 100 | 3.00 | 32991 | 34702 |  | 46249 | 6.82 |  |  |  |
|  |  | 150 | 2.00 | 37248 | 39443 |  | 50990 | 7.50 |  |  |  |
|  |  | 250 | 1.20 | 41536 | 44284 |  | 55831 | 8.19 |  |  |  |
|  |  | 500 | 0.60 | 45461 | 48773 |  | 60320 | 8.83 |  |  |  |
|  |  | 750 | 0.40 | 46939 | 50479 |  | 62026 | 9.08 |  |  |  |
|  |  | Unlimited | 0.00 | 50204 | 54275 |  | 65822 | 9.62 |  |  |  |
| 3750 | ```3 6 0 8 with fans: 5 0 5 2``` | 50 | 7.50 | 27234 | 28150 | 14434 | 42583 | 6.29 | $\begin{aligned} & \text { GA40M } \\ & \text { (GA50M) } \end{aligned}$ | GA08E | GA08E |
|  |  | 100 | 3.75 | 37984 | 39790 |  | 54224 | 7.96 |  |  |  |
|  |  | 150 | 2.50 | 43739 | 46151 |  | 60585 | 8.87 |  |  |  |
|  |  | 250 | 1.50 | 49772 | 52919 |  | 67353 | 9.83 |  |  |  |
|  |  | 500 | 0.75 | 55514 | 59459 |  | 73893 | 10.76 |  |  |  |
|  |  | 750 | 0.50 | 57735 | 62014 |  | 76448 | 11.12 |  |  |  |
|  |  | Unlimited | 0.00 | 62755 | 67844 |  | 82278 | 11.95 |  |  |  |
| 5000 | $\begin{array}{r} 4811 \\ \text { with fans: } \\ 6736 \end{array}$ | 50 | 10.00 | 30548 | 31408 | 19245 | 50653 | 7.45 | GA50B | GA32B | GA32B |
|  |  | 100 | 5.00 | 44756 | 46626 |  | 65871 | 9.62 |  |  |  |
|  |  | 150 | 3.33 | 52968 | 55608 |  | 74853 | 10.90 |  |  |  |
|  |  | 250 | 2.00 | 62081 | 65739 |  | 84984 | 12.33 |  |  |  |
|  |  | 500 | 1.00 | 71278 | 76142 |  | 95387 | 13.80 |  |  |  |
|  |  | 750 | 0.67 | 74981 | 80383 |  | 99628 | 14.39 |  |  |  |
|  |  | Unlimited | 0.00 | 83674 | 90458 |  | 109703 | 15.81 |  |  | - |

[^9]Table 3.4: System voltage @480 V - Nominal transformer Z (\%) = $5.75 \pm 7.5 \%$; Minimum transformer $\mathbf{Z}$ (\%) = 5.32
Voltage Rating: 480 V

| Transformer KVA | Full load current <br> (A) | Primary short circuit ${ }^{4}$ (MVA) | $\begin{array}{r} \text { System } \\ \text { Z (\%) } \\ \hline \end{array}$ | Available SC curr. <br> (A), nom. Z | Available SC curr. $\text { (A), } \min \mathrm{Z}$ | Motor contribution, 100\% motor load (A) | Max. combined fault curr. <br> (A) | Arc flash incident energy $\left({ }^{(6)(7)}\right.$ $(\mathrm{cal} / \mathrm{cm} 2)$ | Main $\substack{\text { breaker } \\(1)(2)(3) \\ I_{c w}>I_{s c}}$ | Feeder breaker ${ }^{(5)}$ $\mathrm{I}_{\mathrm{cw}} \leq \mathrm{I}_{\mathrm{cu}}$ | $\begin{array}{r} \text { Feeder } \\ \text { breaker } \\ I_{\mathrm{cw}}=I_{\mathrm{cu}} \text { or } \\ I_{\mathrm{cw}}>I_{\mathrm{sc}} \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 500 | $601$ <br> with fans: $842$ | 50 | 1.00 | 8910 | 9518 | 2406 | 11923 | 1.48 | $\begin{array}{r} \text { GA08E } \\ (\text { GA16E) } \end{array}$ | GN08S | GN08S |
|  |  | 100 | 0.50 | 9623 | 10336 |  | 12741 | 1.57 |  |  |  |
|  |  | 150 | 0.33 | 9886 | 10640 |  | 13046 | 1.61 |  |  |  |
|  |  | 250 | 0.20 | 10108 | 10898 |  | 13303 | 1.63 |  |  |  |
|  |  | 500 | 0.10 | 10280 | 11099 |  | 13504 | 1.66 |  |  |  |
|  |  | 750 | 0.07 | 10339 | 11167 |  | 13573 | 1.66 |  |  |  |
|  |  | Unlimited | 0.00 | 10459 | 11307 |  | 13713 | 1.68 |  |  |  |
| 750 | $\begin{array}{r} 902 \\ \text { with fans: } \\ 1263 \end{array}$ | 50 | 1.50 | 12443 | 13230 | 3608 | 16838 | 2.02 | $\begin{array}{r} \text { GA16E } \\ (\mathrm{GA16E}) \end{array}$ | GN08S | GN08S |
|  |  | 100 | 0.75 | 13879 | 14865 |  | 18473 | 2.20 |  |  |  |
|  |  | 150 | 0.50 | 14434 | 15503 |  | 19112 | 2.26 |  |  |  |
|  |  | 250 | 0.30 | 14911 | 16055 |  | 19664 | 2.32 |  |  |  |
|  |  | 500 | 0.15 | 15290 | 16496 |  | 20104 | 2.37 |  |  |  |
|  |  | 750 | 0.10 | 15421 | 16648 |  | 20256 | 2.39 |  |  |  |
|  |  | Unlimited | 0.00 | 15689 | 16961 |  | 20569 | 2.42 |  |  |  |
| 1000 | $\begin{array}{r} 1203 \\ \text { with fans: } \\ 1684 \end{array}$ | 50 | 2.00 | 15520 | 16435 | 4811 | 21246 | 2.49 | $\begin{gathered} \text { GA16E } \\ (\text { GA20E) } \end{gathered}$ | GN08S | GN08S |
|  |  | 100 | 1.00 | 17819 | 19036 |  | 23847 | 2.76 |  |  |  |
|  |  | 150 | 0.67 | 18745 | 20096 |  | 24907 | 2.87 |  |  |  |
|  |  | 250 | 0.40 | 19558 | 21033 |  | 25844 | 2.97 |  |  |  |
|  |  | 500 | 0.20 | 20215 | 21795 |  | 26606 | 3.05 |  |  |  |
|  |  | 750 | 0.13 | 20444 | 22062 |  | 26873 | 3.08 |  |  |  |
|  |  | Unlimited | 0.00 | 20918 | 22615 |  | 27426 | 3.14 |  |  |  |
| 1500 | $\begin{array}{r} 1804 \\ \\ \text { with fans: } \\ 2526 \end{array}$ | 50 | 3.00 | 20620 | 21689 | 7217 | 28905 | 3.29 | $\begin{array}{r} \text { GA20E } \\ (\text { GA32N }) \end{array}$ | GN08S | GN08S |
|  |  | 100 | 1.50 | 24886 | 26460 |  | 33677 | 3.77 |  |  |  |
|  |  | 150 | 1.00 | 26729 | 28553 |  | 35770 | 3.98 |  |  |  |
|  |  | 250 | 0.60 | 28413 | 30483 |  | 37700 | 4.18 |  |  |  |
|  |  | 500 | 0.30 | 29822 | 32111 |  | 39328 | 4.34 |  |  |  |
|  |  | 750 | 0.20 | 30323 | 32693 |  | 39909 | 4.40 |  |  |  |
|  |  | Unlimited | 0.00 | 31378 | 33922 |  | 41139 | 4.52 |  |  |  |
| 2000 | $\begin{array}{r} 2406 \\ \text { with fans: } \\ 3368 \end{array}$ | 50 | 4.00 | 24673 | 25815 | 9623 | 35437 | 3.95 | $\begin{array}{r} \text { GA32N } \\ \text { (GA4OM) } \end{array}$ | GN08S | GN08N |
|  |  | 100 | 2.00 | 31040 | 32869 |  | 42492 | 4.65 |  |  |  |
|  |  | 150 | 1.33 | 33962 | 36163 |  | 45786 | 4.97 |  |  |  |
|  |  | 250 | 0.80 | 36727 | 39316 |  | 48938 | 5.28 |  |  |  |
|  |  | 500 | 0.40 | 39116 | 42066 |  | 51688 | 5.55 |  |  |  |
|  |  | 750 | 0.27 | 39983 | 43070 |  | 52692 | 5.64 |  |  |  |
|  |  | Unlimited | 0.00 | 41837 | 45229 |  | 54852 | 5.85 |  |  |  |


| Transformer KVA | Full load current <br> (A) | Primary short sircuit ${ }^{4}$ (MVA) | $\begin{gathered} \text { System } \\ \mathrm{Z} \text { (\%) } \\ \hline \end{gathered}$ | Available SC Curr. <br> (A), Nom. Z | Available SC curr. (A), $\min Z$ | Motor contribution, 100\% motor load (A) | Max. combined fault curr. <br> (A) | $\begin{array}{r} \text { Arc flash } \\ \text { incident } \\ \text { energy }{ }^{(6)(7)} \\ (\mathrm{cal} / \mathrm{cm} 2) \end{array}$ | Main breaker <br> (1)(2)(3) $I_{c w}>I_{s c}$ | Feeder breaker ${ }^{(5)}$ $\mathrm{I}_{\mathrm{cw}} \leq \mathrm{I}_{\mathrm{cu}}$ | $\begin{array}{r} \text { Feeder } \\ \text { breaker }{ }^{(5)} \\ I_{\mathrm{cw}}=I_{\mathrm{cu}} \text { or } \\ I_{\mathrm{cw}}>I_{\mathrm{sc}} \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2500 | $\begin{array}{r} 3007 \\ \text { with fans: } \\ 4210 \end{array}$ | 50 | 5.00 | 27972 | 29141 | 12028 | 41170 | 4.52 | $\begin{array}{r} \text { GA32N } \\ \text { (GA50M) } \end{array}$ | GN08H | GA08E |
|  |  | 100 | 2.50 | 36449 | 38459 |  | 50487 | 5.43 |  |  |  |
|  |  | 150 | 1.67 | 40544 | 43047 |  | 55075 | 5.87 |  |  |  |
|  |  | 250 | 1.00 | 44549 | 47589 |  | 59617 | 6.31 |  |  |  |
|  |  | 500 | 0.50 | 48113 | 51678 |  | 63706 | 6.70 |  |  |  |
|  |  | 750 | 0.33 | 49431 | 53202 |  | 65230 | 6.84 |  |  |  |
|  |  | Unlimited | 0.00 | 52296 | 56536 |  | 68565 | 7.15 |  |  |  |
| 3000 | $\begin{array}{r} 3608 \\ \text { with fans: } \\ 5052 \end{array}$ | 50 | 6.00 | 30710 | 31880 | 14434 | 46314 | 5.03 | $\begin{aligned} & \text { GA40M } \\ & \text { (GA50M) } \end{aligned}$ | GN08H | GA08E |
|  |  | 100 | 3.00 | 41239 | 43377 |  | 57811 | 6.14 |  |  |  |
|  |  | 150 | 2.00 | 46561 | 49304 |  | 63738 | 6.70 |  |  |  |
|  |  | 250 | 1.20 | 51920 | 55355 |  | 69789 | 7.27 |  |  |  |
|  |  | 500 | 0.60 | 56826 | 60966 |  | 75400 | 7.79 |  |  |  |
|  |  | 750 | 0.40 | 58674 | 63098 |  | 77532 | 7.99 |  |  |  |
|  |  | Unlimited | 0.00 | 62755 | 67844 |  | 82278 | 8.43 |  |  |  |
| 3750 | with fans:$6315$ | 50 | 7.50 | 34042 | 35187 | 18042 | 53229 | 5.70 | GA50M | GN08P | - |
|  |  | 100 | 3.75 | 47479 | 49737 |  | 67779 | 7.08 |  |  |  |
|  |  | 150 | 2.50 | 54673 | 57689 |  | 75731 | 7.82 |  |  |  |
|  |  | 250 | 1.50 | 62214 | 66149 |  | 84191 | 8.61 |  |  |  |
|  |  | 500 | 0.75 | 69393 | 74324 |  | 92366 | 9.36 |  |  |  |
|  |  | 750 | 0.50 | 72169 | 77517 |  | 95560 | 9.65 |  |  |  |
|  |  | Unlimited | 0.00 | 78444 | 84805 |  | 102847 | 10.31 |  | GA32L |  |

[^10]Table 3.5: System voltage @240 V - Nominal transformer Z (\%) = $5.75 \pm 7.5 \%$; Minimum transformer Z (\%) = 5.32
Voltage Rating: 240 V

| Transformer KVA | Full load current <br> (A) | Primary short circuit ${ }^{4}$ (MVA) | $\begin{gathered} \text { System } \\ \text { Z (\%) } \\ \hline \end{gathered}$ | Available SC curr. <br> (A), nom. Z | Available SC curr. (A), min Z | Motor contribution, 100\% motor load (A) | Max. combined fault curr. <br> (A) | ```Arc flash incident energy(6)(7) (cal/cm2)``` | Main breaker (1)(2)(3) $\mathrm{I}_{\mathrm{cw}}>\mathrm{I}_{\mathrm{sc}}$ | $\begin{array}{r} \text { Feeder } \\ \text { breaker } \\ \mathrm{I}_{\mathrm{cw}} \leq \mathrm{I}_{\mathrm{cu}} \end{array}$ | Feeder breaker ${ }^{(5)}$ $\begin{array}{r} I_{\mathrm{cw}}=I_{\mathrm{cu}} \text { or } \\ \mathrm{I}_{\mathrm{cw}}>I_{\mathrm{sc}} \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 500 | 1203 <br> with fans: 1684 | 50 | 1.00 | 17819 | 19036 | 2406 | 21441 | 1.52 | $\begin{aligned} & \text { GA16E } \\ & (\text { GA20E) } \end{aligned}$ | GN08S | GN08S |
|  |  | 100 | 0.50 | 19245 | 20671 |  | 23077 | 1.61 |  |  |  |
|  |  | 150 | 0.33 | 19772 | 21281 |  | 23687 | 1.64 |  |  |  |
|  |  | 250 | 0.20 | 20215 | 21795 |  | 24201 | 1.67 |  |  |  |
|  |  | 500 | 0.10 | 20561 | 22197 |  | 24603 | 1.69 |  |  |  |
|  |  | 750 | 0.07 | 20679 | 22335 |  | 24740 | 1.69 |  |  |  |
|  |  | Unlimited | 0.00 | 20918 | 22615 |  | 25020 | 1.71 |  |  |  |
| 750 | $\begin{array}{r} 1804 \\ \text { with fans: } \\ 2526 \end{array}$ | 50 | 1.50 | 24886 | 26460 | 3608 | 30068 | 1.96 | $\begin{array}{r} \text { GA20E } \\ (\mathrm{GA} 32 \mathrm{~N}) \end{array}$ | GN08S | GN08S |
|  |  | 100 | 0.75 | 27757 | 29730 |  | 33338 | 2.12 |  |  |  |
|  |  | 150 | 0.50 | 28868 | 31007 |  | 34615 | 2.18 |  |  |  |
|  |  | 250 | 0.30 | 29822 | 32111 |  | 35719 | 2.24 |  |  |  |
|  |  | 500 | 0.15 | 30580 | 32991 |  | 36600 | 2.28 |  |  |  |
|  |  | 750 | 0.10 | 30841 | 33296 |  | 36904 | 2.29 |  |  |  |
|  |  | Unlimited | 0.00 | 31378 | 33922 |  | 37530 | 2.32 |  |  |  |
| 1000 | $\begin{array}{r} 2406 \\ \text { with fans: } \\ 3368 \end{array}$ | 50 | 2.00 | 31040 | 32869 | 4811 | 37681 | 2.33 | $\begin{array}{r} \text { GA32N } \\ (\text { GA40M }) \end{array}$ | GN08S | GN08N |
|  |  | 100 | 1.00 | 35639 | 38071 |  | 42882 | 2.57 |  |  |  |
|  |  | 150 | 0.67 | 37490 | 40191 |  | 45003 | 2.66 |  |  |  |
|  |  | 250 | 0.40 | 39116 | 42066 |  | 46877 | 2.75 |  |  |  |
|  |  | 500 | 0.20 | 40431 | 43590 |  | 48401 | 2.81 |  |  |  |
|  |  | 750 | 0.13 | 40889 | 44123 |  | 48934 | 2.84 |  |  |  |
|  |  | Unlimited | 0.00 | 41837 | 45229 |  | 50040 | 2.88 |  |  |  |
| 1500 | ```3 6 0 8 with fans: 5 0 5 2``` | 50 | 3.00 | 41239 | 43377 | 7217 | 50594 | 2.91 | $\begin{array}{r} \text { GA40M } \\ (\text { GA50M }) \end{array}$ | GNO8H | GA08E |
|  |  | 100 | 1.50 | 49772 | 52919 |  | 60136 | 3.31 |  |  |  |
|  |  | 150 | 1.00 | 53458 | 57107 |  | 64324 | 3.49 |  |  |  |
|  |  | 250 | 0.60 | 56826 | 60966 |  | 68183 | 3.64 |  |  |  |
|  |  | 500 | 0.30 | 59644 | 64221 |  | 71438 | 3.77 |  |  |  |
|  |  | 750 | 0.20 | 60646 | 65385 |  | 72602 | 3.82 |  |  |  |
|  |  | Unlimited | 0.00 | 62755 | 67844 |  | 75061 | 3.92 |  |  |  |
| 2000 | $\begin{array}{r} 4811 \\ \text { with fans: } \\ 6736 \end{array}$ | 50 | 4.00 | 49346 | 51630 | 9623 | 61252 | 3.36 | GA50B | GN08P | GA32B |
|  |  | 100 | 2.00 | 62081 | 65739 |  | 75361 | 3.93 |  |  |  |
|  |  | 150 | 1.33 | 67924 | 72327 |  | 81950 | 4.19 |  |  |  |
|  |  | 250 | 0.80 | 73454 | 78631 |  | 88254 | 4.43 |  |  |  |
|  |  | 500 | 0.40 | 78232 | 84131 |  | 93754 | 4.63 |  |  |  |
|  |  | 750 | 0.27 | 79965 | 86140 |  | 95762 | 4.71 |  |  |  |
|  |  | Unlimited | 0.00 | 83674 | 90458 |  | 100081 | 4.87 |  |  | - |

[^11]Table 3.6: System voltage @208 V - Nominal transformer Z (\%) = $5.75 \pm 7.5 \%$; Minimum transformer $\mathbf{Z}$ (\%) = 5.32
Voltage Rating: 208 V

| Transformer KVA | Full load current <br> (A) | Primary short circuit ${ }^{4}$ (MVA) | $\begin{array}{r} \text { System } \\ \text { Z (\%) } \\ \hline \end{array}$ | Available SC curr. (A), nom. Z | Available SC curr. $\text { (A), } \min Z$ | Motor contribution, 100\% motor load (A) | Max. combined fault curr. <br> (A) | $\begin{array}{r} \text { Arc flash } \\ \text { incident } \\ \text { energy }{ }^{(6)(7)} \\ (\mathrm{cal} / \mathrm{cm} 2) \end{array}$ | Main breaker (1)(2)(3) $I_{c w}>I_{s c}$ | Feeder breaker ${ }^{(5)}$ $\mathrm{I}_{\mathrm{cw}} \leq \mathrm{I}_{\mathrm{cu}}$ | $\begin{array}{r} \text { Feeder } \\ \text { breaker } \\ I_{\mathrm{cw}}=I_{\mathrm{cc}} \text { or } \\ I_{\mathrm{cw}}>I_{\mathrm{sc}} \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 500 | $\begin{array}{r} 1388 \\ \text { with fans: } \\ 1943 \end{array}$ | 50 | 1.00 | 20561 | 21964 | 2776 | 24740 | 1.22 | $\begin{aligned} & \text { GA16E } \\ & (\mathrm{GA} 20 \mathrm{E}) \end{aligned}$ | GN08S | GN08S |
|  |  | 100 | 0.50 | 22206 | 23852 |  | 26627 | 1.29 |  |  |  |
|  |  | 150 | 0.33 | 22814 | 24555 |  | 27331 | 1.31 |  |  |  |
|  |  | 250 | 0.20 | 23325 | 25148 |  | 27924 | 1.33 |  |  |  |
|  |  | 500 | 0.10 | 23724 | 25612 |  | 28388 | 1.35 |  |  |  |
|  |  | 750 | 0.07 | 23860 | 25771 |  | 28546 | 1.35 |  |  |  |
|  |  | Unlimited | 0.00 | 24137 | 26094 |  | 28869 | 1.36 |  |  |  |
| 750 | $\begin{array}{r} 2082 \\ \text { with fans: } \\ 2915 \end{array}$ | 50 | 1.50 | 28714 | 30530 | 4164 | 34694 | 1.56 | $\begin{array}{r} \text { GA2OE } \\ (\text { GA32N }) \end{array}$ | GN08S | GN08S |
|  |  | 100 | 0.75 | 32028 | 34303 |  | 38467 | 1.69 |  |  |  |
|  |  | 150 | 0.50 | 33309 | 35777 |  | 39941 | 1.73 |  |  |  |
|  |  | 250 | 0.30 | 34410 | 37051 |  | 41214 | 1.77 |  |  |  |
|  |  | 500 | 0.15 | 35285 | 38067 |  | 42231 | 1.81 |  |  |  |
|  |  | 750 | 0.10 | 35586 | 38418 |  | 42582 | 1.82 |  |  |  |
|  |  | Unlimited | 0.00 | 36205 | 39141 |  | 43304 | 1.84 |  |  |  |
| 1000 | $\begin{array}{r} 2776 \\ \text { with fans: } \\ 3886 \end{array}$ | 50 | 2.00 | 35816 | 37926 | 5551 | 43478 | 1.84 | $\begin{array}{r} \text { GA32E } \\ (\text { GA40M }) \end{array}$ | GN08N | GN08N |
|  |  | 100 | 1.00 | 41122 | 43928 |  | 49480 | 2.03 |  |  |  |
|  |  | 150 | 0.67 | 43258 | 46375 |  | 51926 | 2.10 |  |  |  |
|  |  | 250 | 0.40 | 45134 | 48537 |  | 54089 | 2.17 |  |  |  |
|  |  | 500 | 0.20 | 46651 | 50296 |  | 55848 | 2.22 |  |  |  |
|  |  | 750 | 0.13 | 47179 | 50911 |  | 56463 | 2.24 |  |  |  |
|  |  | Unlimited | 0.00 | 48273 | 52187 |  | 57739 | 2.27 |  |  |  |
| 1500 | $\begin{array}{r} 4164 \\ \text { with fans: } \\ 5829 \end{array}$ | 50 | 3.00 | 47584 | 50051 | 8327 | 58378 | 2.29 | GA50B | GN08P | GA32B |
|  |  | 100 | 1.50 | 57429 | 61061 |  | 69388 | 2.60 |  |  |  |
|  |  | 150 | 1.00 | 61683 | 65893 |  | 74220 | 2.73 |  |  |  |
|  |  | 250 | 0.60 | 65568 | 70346 |  | 78673 | 2.85 |  |  |  |
|  |  | 500 | 0.30 | 68820 | 74102 |  | 82429 | 2.95 |  |  |  |
|  |  | 750 | 0.20 | 69976 | 75444 |  | 83771 | 2.99 |  |  |  |
|  |  | Unlimited | 0.00 | 72410 | 78281 |  | 86608 | 3.06 |  |  |  |

[^12]
## EntelliGuard G low voltage circuit breakers watts lost

Breaker watts loss values (Table 3.7) are shown for 100\% current values. To convert watts loss to BTU/ hour, multiply watts by 3.42. Breaker watts loss for lower current values may be estimated by the following formula:
$W_{\mathrm{e}}=\mathrm{W}_{\mathrm{FL}}\left(\mathrm{I} / \mathrm{I}_{\mathrm{FL}}\right)^{2}$
where:
We = estimated watts loss at load current
WFL = estimated watts loss at full load current ( $100 \%$ of frame rating, see Table 3.7)
I = load current
IFL = full load current (100\% frame rating)

See the watts loss data in Table 3.8 for bus in vertical sections.

Table 3.7: EntelliGuard G LVPCB estimated watts loss (per breaker, 3-pole)

| Breaker <br> frame size | Breaker <br> type | Breaker <br> envelope | Watts loss |
| :--- | ---: | ---: | ---: |
| 800 | $\mathrm{~S} / \mathrm{N} / \mathrm{H} / \mathrm{P}$ | 1 | 58 |
|  | $\mathrm{E} / \mathrm{M}$ | 2 | 45 |
| 1200 | S | 1 | 140 |
| 1600 | $\mathrm{~N} / \mathrm{H}$ | 1 | 230 |
|  | $\mathrm{E} / \mathrm{M}$ | 2 | 180 |
| 2000 | $\mathrm{~N} / \mathrm{H}$ | 1 | 360 |
| 3200 | $\mathrm{E} / \mathrm{M}$ | 2 | 281 |
| 4000 | $\mathrm{~N} / \mathrm{E} / \mathrm{M}$ | 2 | 558 |
| 5000 | $\mathrm{~B} / \mathrm{L}$ | 3 | 318 |
| 6000 | $\mathrm{M} / \mathrm{B} / \mathrm{L}$ | 3 | 498 |

## Ground fault protection

Several types of ground fault protection are available in AKD-20 switchgear using the EntelliGuard TU trip unit and current sensors. Solidly grounded systems will use either a simple current summation for individual branch feeder circuit breakers or a modified differential scheme for multiple source systems.

Ground fault for 3-wire branch circuits is accomplished by summing the phase currents from the integral current sensors on the circuit breaker. Branch circuit breakers serving 4-wire loads require the addition of a neutral current sensor (Rogowski coil) to monitor the load neutral current.

The signal from the neutral Rogowski coil is added to the trip unit summation circuit through the breaker secondary disconnect. Main and tie circuit breakers used on solidly grounded, 3-wire systems (no neutral bus for branch circuit loads) may also use the same summation ground fault protection system. Trip unit setup is under the heading of "GF SUM."

Table 3.8: Low voltage switchgear bussing estimated watts loss (per section, 3-phase)

| Section Width (in.) | Main bus rating (A) | Watts loss |
| :---: | :---: | :---: |
| 22 | 2000 | 743 |
|  | 3200 | 1420 |
|  | 4000 | 1893 |
|  | 5000 | 2014 |
|  | 6000 | 2163 |
|  | 8000 | 2698 |
| 30 | 2000 | 802 |
|  | 3200 | 1535 |
|  | 4000 | 2044 |
|  | 5000 | 2209 |
|  | 6000 | 2413 |
|  | 8000 | 3142 |
| 34 | 2000 | 831 |
|  | 3200 | 1592 |
|  | 4000 | 2120 |
|  | 5000 | 2307 |
|  | 6000 | 2538 |
|  | 8000 | 3364 |
| 38 | 2000 | 499 |
|  | 3200 | 1103 |
|  | 4000 | 1597 |
|  | 5000 | 2298 |
|  | 6000 | 2931 |
|  | 8000 | 3854 |

Multiple-source systems (or single-source systems with provisions for additional sources) with a neutral bus for branch circuit loads require the use of a modified differential ground fault scheme. The modified differential ground fault scheme, shown in Figure 3.1 for a typical double-ended substation configuration, accommodates neutral-to-ground bonding at each source. The scheme monitors all phase and neutral conductors on all source and tie circuit breakers and accounts for ground current flowing on the neutral bus due to the common neutral connection between sources.

The interconnection of the current sensors also accommodates any neutral load current that may appear on the ground bus. Each source and tie circuit breaker will have three standard 5 A relaying-type current transformers mounted in the breaker cassette and a similar current transformer mounted on the neutral conductor. The secondary of these four current transformers are connected to a summing CT in the breaker section.

For simplicity, the four phase and neutral current transformers and summing CT are represented by a single current transformer symbol on the three-line diagram (Figure 3.1). The secondary of the summing CTs are interconnected to allow unbalanced currents to circulate in the loop. Trip units for the source and tie breakers are connected to the summing CT loop through individual auxiliary current transformers. The summing and auxiliary current transformers are designed to allow a mixture of phase current transformer ratings for the source and tie breakers. For example, in the double-ended substation, below, one main circuit breaker may be rated 4000 A, the other main rated 3200 A and the tie circuit breaker may be rated 2000 A.

The summing and auxiliary CT ratios allow the use of phase and neutral current transformers that match the breaker frame rating rather than requiring all current transformers to have the same primary rating.

For ground faults on branch circuits, the multisource ground fault scheme will provide backup tripping for the feeder circuit breaker ground fault protection. The source and tie breakers that are connected to the bus with the ground fault will be signaled to trip should the feeder breaker fail to clear the ground fault. The same tripping response applies if the ground fault is ahead of the branch circuit breaker, within the switchgear, or on interconnecting cables or busway for multisource systems that are split into multiple lineups. The faulted bus section will be isolated by tripping the source and tie breakers connected to the bus. Trip unit setup is under the heading of "GF CT." All of the trip unit ground fault functions can be specified either to trip the circuit breaker or to provide an alarm when a ground fault is sensed. All ground fault tripping is self-powered and requires no shunt trip coil or control power source. Ground fault alarms require either a Modbus connection to the trip unit or use of the programmable contact on the trip unit and a powered alarm circuit.


Figure 3.1: Example ground fault diagram

## Ground detector considerations

High-resistance pulsing ground detection system This system provides a means for grounding the neutral of a power system, utilizing the "highresistance" method. It allows the switchgear to operate as an "ungrounded" system but eliminates the danger of high transient overvoltage during certain types of ground faults. For delta systems, a set of grounding transformers is provided for connection of the grounding resistor. Figure 3.2 shows a typical ground system visualization of the devices and operations in the switchgear.


Figure 3.2: Pulsing high-resistance ground detection interface

The pulsing high-resistance ground detection system uses a voltmeter relay with an adjustable set point to detect abnormal ground current through the grounding resistor. A green indicating light shows normal conditions, and a red indicating light indicates the presence of a phase-toground fault. Alarm contacts allow remote indication of the ground condition. The location of the fault is quickly determined using a pulsing current in conjunction with a sensitive clamp-on ammeter, which permits clearing of the ground fault before a second phase-to-ground fault causes an outage. After the fault is located and cleared, the system is reset and ready to detect the next ground fault. The pulsing highresistance ground detection system can be enhanced by the addition of a current sensor on each feeder breaker, connected to individual ammeters on the switchgear front panel. The ammeter provides visual indication of the faulted feeder when the grounding resistor is being pulsed, avoiding the need for a clamp-on ammeter to detect the faulted feeder in the switchgear.

Ground detection on ungrounded systems This system provides visual indication of the presence of a phase-to-ground condition on a delta ungrounded system. Ground detection on ungrounded systems consists of one set of three voltage transformers rated for full phasetophase voltage on the primary winding and 120 V secondary winding. The primary is connected wye. The secondary connection is dependent on the type of ground indicators and alarm devices used. A loading or stabilizing resistor may be used in the voltage transformer primary connection to ground if ferroresonance with the distributed capacitance of the system is an issue. Ground indication and alarm can be accomplished as described in the following tables.

> Caution: A combination of ground indication and metering or relaying on the same set of voltage transofrmers is not recommended. Metering not only may require different primary and/or secondary connections; It also increases the probability of faults in the secondary circuits with consequent false indications of grounds on the primary system.

Table 3.9: Operation with lights or voltmeters

| Standard | Three 120 V indicating lights with clear <br> lenses (one per phase). Voltage transformers <br> with wye-connected secondaries. |
| ---: | ---: |
| Option | Three voltmeters instead of indicating lights. <br> Voltage transformers with wye-connected <br> secondaries. |
|  |  |

Operational Assuming rated system voltage on the
description primary of the voltage transformers, the three lamps would glow about equally at subnormal brilliancy because the voltage across each lamp is 69.3 V . Similarly, each voltmeter would read 69.3 V . If one phase of the system becomes grounded, the voltage transformer on the grounded phase would be short-circuited, and the other two transformers would rise to approximately full phase-to-phase voltage. The lamp on the grounded phase would be dark, and the other two lamps would glow at normal brilliance. Similarly, the voltmeter on the grounded phase would read zero and the other two voltmeters would read 120 V .

Table 3.10: Operation with alarm relay
\(\left.$$
\begin{array}{l}\text { Option } \begin{array}{r}\text { An overvoltage relay coil rating of } 199 \mathrm{~V} \mathrm{to} \\
208 \mathrm{~V} \text {, pickup range of } 16 \mathrm{~V} \text { to } 64 \mathrm{~V} \text { or } 70 \mathrm{~V} \\
\text { to } 140 \mathrm{~V} \text {. Voltage transformers with broken } \\
\text { delta-connected secondaries. Note that either } \\
\text { indicating lights or voltmeters (Table 3-9) can } \\
\text { be used as ground indicators with this option. }\end{array} \\
\hline \begin{array}{r}\text { Operational } \\
\text { description }\end{array} \\
\begin{array}{r}\text { Operation with the alarm relay is the same as } \\
\text { described in Table 3-9, although the }\end{array}
$$ <br>
connections are different. Assuming rated <br>
system voltage on the voltage transformers' <br>
primary, the three secondary voltage vectors <br>
add up to zero, resulting in no voltage at the <br>
relay. If one phase of the system becomes <br>

grounded, the voltage transformer on the\end{array}\right\}\)| grounded phase would be short-circuited and |
| ---: |
| the other two transformers would rise to full |
| phase-to-phase voltage. The secondary |
| voltages would also rise to the phase-tophase |
| values (120 V). Because these two voltages |
| are in series at an angle of $60^{\circ}$ underground |
| fault conditions, the voltage imposed on the |
| relay is three times the voltage on each |

Table 3.11: Operation with test switch

| Option | Test switch (for either lamp <br> test or test-forground). |
| :--- | ---: |
| Operational <br> description | The lamp test feature is performed using the <br> normally closed contact of the test switch. <br> The test-for-ground feature is performed <br> using the normally open contact. You must <br> specify which test feature <br> is to be furnished. |

## Breaker control systems

Accessories for the EntelliGuard G circuit breaker accommodate control schemes from the very simple to the complex. Electrical safety procedures emphasize the need for controlling breakers from a remote location or control station to keep electricians, operators, and maintenance personnel away from potential arc flash hazards. The need for continuity of service drives designs with multiple sources and automatic transfers to ensure loads remain energized from any available sources.

Switchgear lineups with multiple sources, either doubleended with two utility-fed transformers or a single utility with an emergency generator can be controlled so that a loss of one utility source will cause the main, tie, or generator breakers to open and close, maintaining power to the switchgear buses. Automatic breaker transfer schemes (autotransfer) can be implemented with discrete relays and hard wiring between source and tie breakers or with programmable logic controllers (PLC) for more complex control sequences. While no single standard auto-transfer scheme will meet all customer needs, the AKD-20 switchgear and EntelliGuard G breakers provide flexible equipment configurations, sensing, and controls for almost any requirement. The basic set of components supplied with any auto-transfer scheme include:

- Electrically operated breakers;
- Voltage sensing on the source breakers;
- Lockout for overcurrent trips;
- Breaker position switches;
- Timers;
- An Auto/Manual control selector switch.

Depending on the specific application, additional components may be supplied for bus voltage sensing, synchronism check, generator start/stop signals, open or closed transition return to normal, test switches, and maintenance transfer selector switches.

As a starting point for sequences of operation and typical bills of material, consider 3-breaker (Main-Tie-Main) and 2- breaker (Main-Generator) autotransfer schemes. Following are descriptions of the 3-breaker and 2-breaker automatic transfer schemes, including basic bills of material, transfer scheme options, sequences of operation, and single-line diagrams.

## Main-tie-main (3-breaker) auto-transfer

(Figure 3-3)
Basic bill of material:

- Electrically operated main and tie breakers with bell alarm/lockout, drawout position switch, breaker control switch, and indicating lights;
- Line-side voltage transformers on each main breaker;
- Voltage sensing relays on each main breaker - (1) three-phase voltage sensing relay, Device 27, and (1) phase loss/phase unbalance relay, Device 47N - all DIN rail mounted;
- Auto/Manual selector switch, Device 43;
- Electrical interlocking (hardwired) between main and tie breakers - with and without PLC control;
- Delayed auto-return to normal after utility voltage source returns with open transition (break-beforemake);
- Options for the basic auto-transfer scheme:
- Manual transfer (return) to normal with open transition (break-before-make);
- Delayed auto-return to normal with closed transition (make-before-break) and sync check relay, Device 25;
- Bus-connected voltage transformers for residual voltage sensing;
- Test switch to simulate loss of utility voltage;
- Maintenance transfer trip selector switch (Device 10) to select breaker to trip when all 3 main and tie breakers are closed (system paralleled).

Additional bill of material for PLC/non-PLC control:

- Non-PLC-based transfer;
- Auxiliary relays for voltage sensing (one per voltage relay), Device 27/47X;
- Auxiliary relays for bell alarm (one per main and tie breaker), Device 86X;
- Timers and auxiliary relays for delay on transfer, delay on return, Device 2, 62;
- Auxiliary relay for sync check relay (when closed transition is required and sync check relay is provided), Device 25X;
- PLC-based transfer using intelligent platforms of PLC with non-volatile memory (NVM) and backup UPS;
- Interposing close and trip relays for main and tie breakers (two per main and tie breaker), Device 94, 95;
- Auxiliary relays for bell alarm (one per main and tie breaker), Device 86X;
- Auxiliary relay for sync check relay (when closed transition is required and sync check relay is provided), Device 25X;
- PLC alarm relay, Device 74;
- Option for PLC-based transfer;
- Touch-screen interface for timer adjustment and system feedback.


## Main-tie-main plc auto-transfer sequence of operations

1. Each utility has 3-phase undervoltage sensing and phase loss protection;
2. Closed transition return to normal (option) includes synchronism check relay;
3. PLC includes UPS for back-up control power for CPU and I/O;
4. Auto-transfer blocked when any main or bus tie breaker trips on overcurrent (overload, short circuit, ground fault) or when any main or bus tie breaker is racked out of the CONNECT position;
5. Hardwired electrical interlocking between main and bus tie breakers to prevent parallel operation (only 2 of 3 breakers can be closed at any time standard), unless permitted by sync check relay (optional);
6. Return to normal (both mains closed, bus tie open) after a transfer and utility voltage has been restored will be automatic with time delay and open transition (break-before-make).

Initial Setup

1. Set Auto-Manual switch to Manual position;
2. Close Main1;
3. Close Main2;
4. Bus Tie remains open;
5. Set Auto-Manual switch to Auto position.

Loss of Utility1

1. After preset time delay, verify Utility2 is available;
2. Main1 will open;
3. Bus Tie will close.

Return of Utility1

1. After preset time delay, verify Utility1 is available;
2. Bus Tie will open;
3. Main1 will close (break-before-make).

Loss of Utility2

1. After preset time delay, verify Utility1 is available;
2. Main2 will open;
3. Bus Tie will close.

Return of Utility2

1. After preset time delay, verify Utility2 is available;
2. Bus Tie will open;
3. Main2 will close (break-before-make).

## Option for closed transition return to normal (Make-before-break)

Return of Utility1

1. After preset time delay, verify

Utility1 is available;
2. Verify Utility1 and Utility2 are in sync;
3. Close Main1;
4. After preset time delay Bus Tie will open (make-beforebreak).

Return of Utility2

1. After preset time delay, verify Utility2 is available;
2. Verify Utility1 and Utility2 are in sync;
3. Close Main2;
4. After preset time delay Bus Tie will open (make-beforebreak).

## Option for closed transition maintenance transfer (Make-before-break)

In this configuration, Main1 and Main2 are closed, while the Bus Tie is open.

Transfer all loads to main1 (Bus1 and Bus2) without deenergizingload (bumpless transfer)

1. Set Trip Selector switch to Trip Main2;
2. Verify Utility1 and Utility2 are in synchronism;
3. Close Bus Tie;
4. After preset time delay, Main2 will open, transferring all loads to Main1 (Bus1 and Bus2).

Return loads to each bus

1. Set Trip Selector switch to Trip Bus Tie;
2. Verify Utility1 and Utility2 are in synchronism;
3. Close Main2;
4. After preset time delay, Bus Tie will open, transferring Bus2 loads back to Main2.

Transfer all loads to main2 (Bus1 and Bus2) without deenergizing load (bumpless transfer)

1. Set Trip Selector switch to Trip Main1;
2. Verify Utility1 and Utility2 are in synchronism;
3. Close Bus Tie;
4. After preset time delay, Main1 will open, transferring all loads to Main2 (Bus1 and Bus 2).

Return loads to each bus

1. Set Trip Selector switch to Trip Bus Tie;
2. Verify Utility1 and Utility2 are in synchronism.
3. Close Main1;
4. After preset time delay, Bus Tie will open, transferring Bus1 loads back to Main1.

Option for test switch to simulate utility failure In this configuration, Main1 and Main2 are closed, and the Bus Tie open.

1. Transfer to Side2-Simulates loss of Utility1 and executes automatic transfer as described in Loss of Utility1;
2. Normal - Returns Main1, Main2, and Bus Tie breakers to their normal position based on Open or Close Transition options;
3. Transfer to Side1 - Simulates loss of Utility2 and executes automatic transfer as described in Loss of Utility2.

Option for redundant bus tie breaker (Main-tie-tiemain, Figure 3.4)

1. Redundant bus tie breaker is normally closed and not operated by the PLC;
2. Drawout position switch and bell alarm are provided for inputs to PLC;
3. If redundant bus tie breaker is racked out of the CONNECT position or trips on overcurrent, then the auto transfer will be disabled.


Figure 3.3: Main-tie-main example single-line diagram


## Main-generator (2-breaker) auto-transfer

 (Figure 3-5)Basic bill of material:

- Electrically operated main and generator breakers with bell alarm/lockout, drawout position switch, breaker control switch, and indicating lights;
- Line-side voltage transformers on the main and generator breaker;
- Voltage sensing relays on the main breaker - (1) threephase voltage sensing relay, Device 27, and (1) phase loss/phase unbalance relay, Device 47 N - all DIN rail mounted;
- Voltage and frequency sensing relays on the generator breaker - (1) three-phase voltage sensing relay, Device 27 , and (1) single-phase over-/underfrequency relay, Device 81O/U all DIN rail mounted;
- Auto/Manual selector switch, Device 43
- Electrical interlocking (hardwired) between main and generator breakers - with and without PLC control;
- Delayed auto-return to normal with open transition (break-before-make);
- Generator start/stop signal;
- Options for the basic auto transfer scheme:
- Manual transfer (return) to normal after utility voltage source returns;
- Delayed auto-return to normal with closed transition (make-before-break) and sync check relay;
- Bus-connected voltage transformers for residual voltage sensing;
- Test switch to simulate loss of utility voltage for generator no-load (start/stop) or full load test (autotransfer).

Bill of material for PLC/non-PLC control

- Non-PLC-based transfer;
- Auxiliary relays for voltage and frequency sensing (one per voltage relay), Device 27/47X, 27/81X;
- Auxiliary relays for bell alarm (one per main and generator breaker), Device 86X;
- Timer and auxiliary relay for delay on transfer, delay on return, Device 2, 62;
- Auxiliary relay for sync check relay (when closed transition is required and sync check relay is provided), Device 25X
- PLC-based transfer using intelligent platforms of PLC with non-volatile memory (NVM) and backup UPS;
- Interposing close and trip relays for main and;
- generator breakers (two per main and generator breaker), Device 94, 95;
- Auxiliary relays for bell alarm (one per main and generator breaker), Device 86X;
- Auxiliary relay for sync check relay (when closed transition is required and sync check relay is provided), Device 25X;
- PLC alarm relay, Device 74;
- Option for PLC-based transfer;
- Touchscreen interface for timer adjustment and system feedback.


## Main-generator PLC auto transfer sequence of operations

1. Utility source has 3-phase undervoltage sensing and phase loss protection;
2. Generator source has 3-phase voltage sensing and single-phase frequency sensing;
3. Closed transition return to normal (option) includes synchronism check relay;
4. PLC includes UPS for backup control power for CPU and I/O;
5. Auto-transfer blocked when main or generator breaker trips on overcurrent (overload, short circuit, ground fault) or when main or generator breaker is racked out of the CONNECT position;
6. Hardwired electrical interlocking between main and generator breakers to prevent parallel operation (only 1 of 2 breakers can be closed at any time - standard), unless permitted by sync check relay (optional);
7. Return to normal (main breaker closed, generator breaker open) after a transfer and utility voltage has been restored will be automatic with time delay and open transition (break-before-make).

## Initial Setup

1. Set Auto-Manual switch to Manual position;
2. Close Utility main breaker (52U);
3. Generator breaker (52G) remains open;
4. Set Auto-Manual switch to Auto position.

## Loss of Utility

1. After preset time delay, send start signal to generator;
2. Check for proper voltage and frequency from generator source;
3. After preset time delay with proper voltage and frequency, 52U will open and 52G will close.

Return of Utility

1. Verify utility source is available for preset time delay;
2. 52G will open;
3. After preset time delay, 52U will close (break-beforemake);
4. Remove generator start signal.

## Option for closed transition return to normal (Make- before-break)

Return of Utility

1. Verify utility source is available for preset time delay;
2. Verify utility source and generator source are synchronized;
3. 52U will close;
4. After preset time delay, 52G will open (make-beforebreak);
5. Remove generator start signal.

## Option for test switch to simulate utility failure

In this configuration, 52U is closed and 52G is open.

1. No Load Test - Sends generator start signal;
2. Normal - Returns 52U and 52G breakers to their normal position based on Open or Close Transition options and removes generator start signal;
3. Full Load Test - Simulates loss of utility source and executes automatic transfer as described in Loss of Utility.

## Option for generator cooldown

1. Apply preset time delay after 52G opens before generator start signal is removed.


Figure 3-5: Main-Generator example single-line diagram

AKD-20 switchgear has numerous standard and optional features that can aid in reducing the energy associated with an arc flash or help mitigate the probability of an arc flash incident. Power system design, equipment design, operating procedures, electronics and communications, and new technologies can all be used to address the safety concerns associated with arc flash and shock. It may help if one considers mitigation of the hazards associated with electrical equipment from three perspectives:

- Exposure;
- Probability of an incident during exposure;
- The potential severity of an incident, should it occur.


## Power system design

High resistance grounding (HRG) - limits ground fault current to a detectable level (approximately 5 amperes) while minimizing the possibility of the ground fault escalating to a serious phase to phase arcing fault. The neutral grounding resistor and sensing equipment can be located in the low voltage switchgear, and a pulsing circuit can be added to aid in determining the faulted feeder. HRG is widely considered to minimize the probability of serious faults.

Medium voltage interrupter - use of a circuit breaker or other controllable device that can be tripped in the event of an arcing fault between the transformer secondary terminals and the main secondary breaker. Relays, such as the Multilin F35, F60, T60 (and others), may be used for transformer primary and secondary protection and can accept inputs from CTs located on the transformer secondary.

Implemented with Zone Selective Interlock signals from the low voltage trip unit, such a system can provide full selectivity and instant - or near-instant - protection, and arc flash protection for the conductors between the transformer secondary bushings and the main secondary breaker.

This type of protection can reduce the severity of an incident on the primary connections of the equipment or main bus if no secondary main is used.

## Switchgear equipment design

Insulated/isolated bus - provides an epoxy coating on the horizontal main bus bars and phase isolation barriers in the vertical bus. The vertical bus system is enclosed with polyester-glass barriers. Bolted bus joints are enclosed with removable bus joint covers. Only cable or busway terminations are visible from the rear of the equipment.

The insulated/isolated bus option is available in sections with 800 A to 3200 A breakers (Envelopes 1 and 2 ) with main bus ratings up to, and including, 4000 A .

Bus compartment barriers - bus ratings above 4000 A and sections containing 3200 A to 6000 A (Envelope 3) breakers, can be supplied with bus compartment barriers. These polyester-glass barriers are attached to the switchgear frame and provide a separation between the bus compartment (horizontal and vertical buses) and the cable compartment.

As in the insulated/isolated bus option, the only exposed conductors in breaker sections are cable and busway terminations.

Section barriers - provide a combination of steel and polyester-glass barriers between vertical sections in the cable and bus area. Section barriers limit exposure to terminations in adjacent sections when performing maintenance or trouble-shooting work in the rear of a breaker section. Section barriers are particularly important between the section where a main circuit breaker is housed and sections where feeders are housed to ensure that arc plasma on the main bus does not create an arc on the line side of the main circuit breaker where protection may be much slower.

Shutters - provided as standard on source (main or generator) and tie breakers in multisource switchgear lineups. Shutters operate when the breaker is racked into or out of the cubicle. When the breaker is in the DISCONNECT or WITHDRAWN position, the shutters are closed over the primary disconnects. A padlocking feature allows the shutters to be locked in the closed position when the breaker is out of the cubicle. Optionally, shutters may be supplied on all breakers in the switchgear lineup. Shutters are strongly recommended on all circuit breaker cubicles.

IR windows - may be supplied on the rear doors of the switchgear for IR camera access. Thermal imaging cable terminations in the rear of each switchgear section do not require opening the rear door when the IR windows are supplied. IR windows are strongly recommended to minimize exposure during IR surveys of cable connections.

## Operating the switchgear

Remote control and monitoring - moving operators away from the switchgear to perform monitoring or control functions. Specifying breakers with electric operators (E/O) and shunt trip allows the breaker to be controlled from a location outside the arc flash and arc blast boundaries.

Trip units specified with communication capability (Modbus or Profibus) can provide information about the circuit (metering data) and the circuit breaker (event information, open/close status, trip unit settings) from a safe location away from the front of the switchgear. A touchscreen monitor can be supplied in a switchgear auxiliary compartment or mounted on a wall and provide convenient single-point access to trip unit information for all breakers in the lineup without approaching each individual breaker cubicle.

Remote racking - inserting and withdrawing the circuit breaker from outside the arc flash boundary. After the circuit breaker has been opened via the remote control station and shunt trip on the breaker, the operator can attach the remote racking device to the front of the breaker cubicle. The operator then steps back, up to 30 feet away, from the front of the breaker, sets the controls on the remote racking controller, and proceeds to remotely draw out the breaker from the CONNECT position to the DISCONNECT position.

After the breaker has been removed from the cubicle and any maintenance performed on the breaker, the remote racking device can again be used to remotely rack the breaker back into the CONNECT position. After removing the remote racking device from the front of the breaker cubicle, the operator returns to the remote control station and closes the breaker - from a distance outside the flash and blast boundaries.

## Trip unit electronics

Advances in trip unit technology have made it possible to provide enhanced protection while maintaining the selective tripping functions that switchgear has always been able to provide.

Zone-selective interlocking (ZSI) - digital communication between tiers of circuit breakers to provide increased protection while maintaining selectivity. ZSI allows individual time-delay settings for short time and/or ground fault for "in-zone" and "out-of-zone" faults. An in-zone fault would allow an "unrestrained" (faster) time delay for the upstream (main) breaker, providing better protection for equipment in the zone. An out-ofzone fault would allow the main breaker to operate with a "restrained" (slower) time delay, providing selectivity with the feeder breaker. The feeder breaker initiates the zone selective interlock signal for the out-of-zone fault and clears the fault with minimal service interruption.

ZSI can also be executed with breakers in switchboards or motor control centers, improving protection and selectivity for equipment located downstream of the switchgear.

A further enhancement to ZSI is the addition of Instantaneous ZSI, or I-ZSI, to the breaker trip units. I-ZSI allows an upstream breaker (a main breaker, for example) to trip instantaneously for a fault on the switchgear bus or in a breaker cubicle instead of with a delayed long time or short time trip. This provides vastly improved equipment protection by making the main breaker more sensitive to arcing faults, lowering incident energy levels by tripping the main breaker instantaneously while maintaining selectivity with feeder breakers, on a $7 \times 24$ basis. DET-760 (Guide to Instantaneous Selectivity) describes ABB instantaneous selective circuit breaker offering. Using this guide, it is possible to design a power distribution system, rated up to 100 kA at 480 V that is $100 \%$ selective and provides 100\% instantaneous protection at arcing current levels, $7 \times 24$. Using MV relays such as Multilin F35, F60, or T60, selective instantaneous protection can be extended to the first MV CB ahead of the substations transformer for $100 \%$ selective instantaneous protection of your substation, motor control centers, and panels.

Reduced energy let-through (RELT) - provides a separate, adjustable instantaneous trip function that is enabled by an external Modbus command or remote dry contact. RELT instantaneous trip can be enabled whenever an operator must approach the switchgear or any downstream equipment. RELT on the main breaker provides instantaneous overcurrent protection for the switchgear. RELT on a feeder breaker provides instantaneous overcurrent protection for downstream equipment connected to the feeder. The RELT instantaneous function is $1 / 2$ cycle faster than the normal instantaneous function and can be adjusted as low as 1.5 X of the trip unit rating plug. RELT can affect selectivity so it is normally used only during times when an operator must be in the arc flash boundary.

## New technologies

Arc vault - a remotely activated system that, when triggered by current and voltage signals, will create a secondary arc fault within a containment dome to divert the energy from the arc flash and provide a trip signal to an upstream breaker to clear the fault. The secondary arc fault in the containment dome has a lower impedance than the arcing fault and is therefore able to extinguish the arc fault within 7 msec of the initial event.

When applied to a 480 Volt system with 65 kA available fault current, the Arc Vault is able to reduce incident energy from the arc event to less than $1.2 \mathrm{cal} / \mathrm{cm} 2$ (IEEE 1584, 18 inch working distance), even with the breaker cubicle door open. The Arc Vault section is connected to the protected switchgear lineup via a 2000 A cable connection and can be located up to 50 feet (maximum total cable length) from the switchgear.

Arc flash relay - For applications of Arc Flash systems by ABB or other manufacturers, contact your ABB Application Engineer.

## Entellisys switchgear

We invite you to explore the world of Entellisys low voltage switchgear. Entellisys is a protection and control system that is integrated into the basic AKD-20 structure. In addition to the rugged and time-tested construction of AKD-20, Entellisys low voltage switchgear is the first system to provide the power of knowledge about the entire switchgear lineup. This knowledge can be used by the engineer to improve protection, by the installing contractor to shorten installation time, by the operator to stay out of the arc flash zone, by the maintenance personnel to save maintenance time and money, and by the owner to adapt the equipment to the dynamic needs of the facility. Entellisys helps to reduce costs, shorten schedules, and increase reliability throughout the process of designing, installing, maintaining, and owning your low voltage power distribution switchgear. Figure 4.1 shows the Entellisys architecture.

## Arc flash mitigation

## Easy to add or modify functionality

Information that can impact the power system design is constantly changing. Entellisys' firmwarebased architecture makes it easy for the engineer to modify functionality during almost any portion of the design and build phase without impacting the schedule. This translates to dollars saved. A change in options can be made easily with updated software. And, this flexibility is inherent over the lifetime of the equipment, allowing the owner to continue to meet the changing needs of the facility over time.

## Finally, a holistic approach to low voltage switchgear dynamics

Traditional switchgear trip systems can react only to what they know - the current magnitude and time for one particular circuit. Entellisys is the first circuit-protection technology that overcomes this limitation.

The Entellisys "Single Processor Concept" bases control of every circuit breaker in the switchgear upon what is best for the entire lineup under the exact conditions in the system at that moment. With Entellisys, each circuit breaker is controlled with full information about every current, voltage, and circuit breaker in the switchgear.

## Don't trade selectivity for protection

Entellisys knows the magnitude and the location of a fault. As a result, when Zone Selective Interlocking and Bus Differential are applied, you achieve both fast protection (detection as fast as 0.25 ms ) and selectivity. You can now have the best of both worlds: fast protection while minimizing outage potential.

## Installation and startup

## Fast installation

Entellisys-streamlined architecture minimizes wiring and shipping split terminations by reducing the amount of wiring in equipment - in some cases up to $70 \%$. Consequently, it is efficient and fast to install the Entellisys equipment.

## Faster startup using diagnostics for troubleshooting

The sequence of event logs in Entellisys provides a detailed history of the system dynamics with a resolution of 0.5 ms . Instead of guessing at what might be occurring, personnel can quickly discern exactly what is happening and quickly remedy the situation.

## Streamlined interface to communication systems

Traditional switchgear using discrete devices forces the integrator to interface with many devices within each switchgear lineup. Entellisys streamlines the integration process in a number of ways. Only one interface is required for the entire lineup. That means, instead of interfaces for each type of devices, one interface to the Modbus register map provides access to thousands of registers for data collection as well as control.

## System Operation

## Increased reliability

Since power distribution systems provide continuity of service, Entellisys architecture provides increased reliability when compared to traditional switchgear.

Traditional switchgear has many devices for monitoring, protection, and control over miles of wire. Entellisys has one set of hardware to provide the entire range of possible needed functionality. This simplicity (fewer components, less wiring) increases reliability. Traditional switchgear almost always has a single level of device functionality. Entellisys features redundant central processing units, communication buses, and UPSs as standard.

Traditional switchgear doesn't necessarily know that a function is not working until it is called upon to act. Entellisys is continuously monitoring the health of the system components and, should something not be functioning properly, the instance is identified by the system health screen, the event log, or can be configured as an alarm. The alarms can be emailed to as many as four addresses, providing immediate feedback that attention is needed.

## Increase system availability

What matters to you is that your switchgear is performing as needed providing the protection, monitoring and control for your facility. With the redundant systems and system health monitoring, you are notified should something need to be addressed. Due to the redundant architecture, it is possible to service the system-level devices and maintain service - not something you typically even know about in traditional switchgear, let alone resolve in a nonintrusive manner.

## Decrease downtime using low voltage switchgear diagnostics

Power systems are dynamic, and - prior to Entellisys - it was very hard to determine what exactly had occurred during a disturbance. In traditional systems you may have some trip type indication, possibly a waveform on a circuit or two, and some type of time-stamping that may not be synchronized across devices. Entellisys provides a detailed log of all of the system's protection functions (pick-up, drop-out, etc.), as well as detailed fault reports providing the current and voltage for every EntelliGuard E circuit breaker at the time of the event. An industry first, Entellisys' waveform capture records the current and voltage waveforms for every EntelliGuard E circuit breaker, as well as the open and close commands and actions. All of the events, data, and waveforms are synchronized to within 0.5 ms , providing you with a detailed chronological log of system dynamics. This is a powerful tool in determining exactly what occurred during a disturbance. Entellisys also provides various information as well as protective alarm settings to provide warnings of possible unfavorable conditions, allowing you to take action and prevent an outage. There are real-world examples of how Entellisys identified issues that prevented an outage, as well as provided information to root-cause system conditions.

## Reduced arc-flash hazard

Entellisys offers advanced protection modes known as zone-based protection, which includes bus differential, dynamic zone-selective interlocking, and multi-source ground fault protection. This protection enables fast (as fast as 25 ms ) detection of arcing faults in the equipment while maintaining selectivity. Consequently, the energy letthru from a fault is significantly reduced across the entire range of perspective fault magnitudes. This reduction can mean less cumbersome personal protective equipment (PPE) for the operators, as well as less potential damage to downstream equipment.

Redundant HMI


[^13]
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## Move operators outside the flash protection boundary

The Control Stack allows for the complete interaction with the Entellisys System. The touchscreen display can be placed outside the Flash Protection Boundary. The operator can fully interact with the Entellisys system, view all parameters, and open and close circuit breakers without being in front of live equipment.

## Move operators away from the gear during Rack-in/Rack-out operations

Entellisys' remote racking device eliminates the need for operators to stand in front of a moving circuit breaker during racking-out or racking-in of an EntelliGuard circuit breaker.

## Efficient remote communications

Entellisys provides enhanced communication capabilities for the operator. Alarms can be easily configured and can be emailed to up to four different email addresses. Entellisys communicates all status data, alarms, metering, event logs, etc., digitally over Modbus TCP/IP. The amount of information available, all synchronized, is unprecedented.

## System operation

## Streamlined circuit breaker testing

The Entellisys architecture of circuit hardware (current sensors and messengers) located in the equipment and not on the circuit breaker translates to efficient maintenance procedures for testing. Traditional low voltage power circuit breaker testing requires high-current injection testing. This was a time consuming process, which also increased the probably of damage or an arcing fault due to the movement and handling of the circuit breaker in and out of the gear. Entellisys changes this. The current sensors integrity can be determined by simply reading the metering information on the HMI for each circuit (Figure 4.2). Using the Entellisys test kit, automated or customized test cases are performed with the breaker still in the cubicle. Consequently, EntelliGuard circuit breakers do not require high-current injection testing, saving time and resources while providing comprehensive testing.

## Predictive maintenance information

Entellisys provides circuit breaker operating data so you can improve your maintenance timing. For each circuit breaker, Entellisys tracks the number of various types of operations as well as the date of the last circuit breaker operation. Entellisys also calculates the percentage of the total load life that has been used, both mechanically and electrically. Entellisys can activate alarms and associated emails for various stages during mechanical and electrical life. Now you have data to determine the maintenance required instead of just a time-based system.

Entellisys is the preferred solution in critical applications such as medical center, data centers, water/wastewater plants, petrochem facilities, and airports around the world. State-of-the-art protection, monitoring, and control make it the intelligent choice to provide reliable power distribution now and in the future.


Figure 4.2: Entellisys remote HMI

AKD-20
Sizing and dimensional data

AKD-20 switchgear has numerous standard
configurations with and without optional features.
Figures 5.1 through 5.11, show the layouts for these configuration arrangements and dimensions.


Figure 5.1: Switchgear layout and sizing: $22^{\prime \prime}, 30^{\prime \prime}$, and $34^{\prime \prime}$ sections



Figure 5.3: Switchgear layout and sizing: $22^{\prime \prime}, 30^{\prime \prime}$, and 34 " sections


Figure 5.4: Switchgear layout and sizing: 30 " and 34 " sections


Figure 5.5: Switchgear layout and sizing: 30 " and 34 " sections


Figure 5.6: Switchgear layout and sizing: 34 " sections


Figure 5.7: Switchgear layout and sizing: 34 " sections


Figure 5.8: Switchgear layout and sizing: 34 " sections



Figure 5.10: Switchgear layout and sizing: 38 " sections


Figure 5.11: Switchgear layout and sizing: 38 " sections

## Section views and cable lug landings for feeder

 breakers and main cable feeds
## Cable terminations

Cables used for low voltage power circuit breaker terminations in AKD-20 (with the exception of non-AR breakers rated 2000A or less) must have minimum $90^{\circ} \mathrm{C}$ insulation while the cable ampacity will be based on a $75^{\circ} \mathrm{C}$ rating. This meets the requirements of ANSI C37.20.1, UL1558 and the National Electrical Code. Refer to the example for typical cable ampacities (derating factors that may apply are not shown). Figure 5.12 shows four-high feeder breaker sections and runback locations with and without optional $45^{\circ}$ lug adapters for cables above or below.

| Cable Size | $\mathbf{9 0}^{\circ} \mathbf{C}$ rating (ref.) | $\mathbf{7 5}^{\circ} \mathbf{C}$ rating (of $\mathbf{9 0}^{\circ} \mathbf{C}$ cable) |
| :--- | ---: | ---: |
| 500 kcmil | 430 Amps | 380 Amps |
| 600 kcmil | 475 Amps | 420 Amps |

Example(from NEC table 310.16)


Figure 5.12: Feeder breaker cable termination sections: 800 A-2000 A breaker

Figure 5.13 shows a 2000 A main breaker cable feed with cables to the upper primary disconnects and main bus to the lower primary disconnects. The main bus is in the mid or lower bus position.


Figure 5.13: Main-Tie breaker cable termination sections: 800 A - 2000 A breaker, mid or lower bus

Figure 5.14 shows a 2000 A main breaker cable feed with cables to the upper primary disconnects and main bus to the lower primary disconnects. The main bus is in the lower bus position.


Figure 5.14: Main-Tie breaker cable termination sections: 800 A - 2000 A breaker, lower bus

Figure 5.15 shows a 3200 A or 4000 A main breaker cable feed with cables to the upper or lower primary disconnect. Cables to the upper primary disconnect, main bus in the lower bus position.
Cables to the lower primary disconnect, main bus in the upper or mid bus position.


Figure 5.15: Main-Tie breaker cable termination sections: 3200 A/4000 A breaker

Figure 5.16 shows a 3200 A or 4000 A main breaker cable feed with cables to the upper or lower primary disconnect. Cables to the upper primary disconnect, main bus in the mid or lower bus position. Cables to the lower primary disconnect, main bus in the upper bus position.


Figure 5.16: Main-Tie breaker cable termination sections: 3200 A/4000 A breaker

Figure 5.17 shows a 3200 A or 4000 A main breaker cable feed with cables to the upper or lower primary disconnect. Cables to the upper primary disconnect, main bus in the lower bus position. Cables to the lower primary disconnect, main bus in the upper bus position.


Figure 5.17: Main-Tie breaker cable termination sections: 3200 A/4000 A breaker

Figure 5.18 shows a 5000 or 6000 A main breaker cable feed with cables to the upper or lower primary disconnect. Cables to the upper primary disconnect, main bus in the lower bus position. Cables to the lower primary disconnect, main bus in the upper bus position.


Figure 5.18: Main-Tie breaker cable termination sections: 5000-6000 A breaker

Figure 5.19 shows a 5000-6000 A main breaker cable feed with cables to the upper or lower primary disconnect. Cables to the upper primary disconnect, main bus in the lower bus position.
Cables to the lower primary disconnect, main bus in the upper bus position. Minimum depth is 74 ".


Figure 5.19: Main-Tie breaker cable termination sections:
5000-6000 A breaker

Table 5.1: Feeder breaker cable termination provisions (refer to Figure 5.12)*

| Breaker ampere frame | Compression lugs 600 kcmil and smaller |  |  |  | Clamp (screw) lugs 600 kcmil and smaller |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NEMA 2-Hole drilling |  |  |  |  |  | NEMA 2-Hole drilling |  |
|  | A,B,C-COMP'T |  |  | D-COMPT | A,B,C-COMP'T |  |  | D-COMPT |
|  | $45^{\circ}$ Lug adapter | $90^{\circ} \mathrm{Lug}$ adapter | $45^{\circ}$ Lug adapter | $90^{\circ}$ Lug adapter | $45^{\circ}$ Lug adapter | $90^{\circ}$ Lug adapter | $45^{\circ}$ Lug <br> adapter | $90^{\circ}$ Lug adapter |
| 800 A |  |  |  |  |  |  |  |  |
| 1600 A | 8 | 8 | 6 | 8 | 8 | 8 | 3 | 5 |
| 2000 A |  |  |  |  |  |  |  |  |

* Maximum quantity of lugs shown. Adapter bars are provided for customer-specified quantity of lugs per breaker.

Table 5.2: Main cable feed and bus tap-off (refer to Figure 5.13 through Figure 5.19)

| Breaker frame/ cable tapoff | Compression lugs 600 kcmil and smaller NEMA 2-Hole drilling |  |  | Clamp (screw) lugs 600 kcmil and smaller NEMA 2-Hole drilling |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cable feed/Tapoff location |  |  |  | Cable feed/Tapoff location |  |
|  | Top | Center | Bottom | Top | Center | Bottom |
| 2000 A | 6 (22") | 6 (22") | 6 (22") | 6 (22") | 6 (22") | 6 (22") |
|  | 9 (30") | 9 (30") | 9 (30") | 9 (30") | 9 (30") | 9 (30") |
| 3200 A | 12 | 12 | 12 | 11 | 11 | 11 |
| 4000 A | 12 | - | 12 | 11 | - | 11 |
| 5000 A | 14 | - | 14 | 14 | - | 14 |
| 6000 A | 14 | - | 14 | 14 | - | 14 |

Figures 5.21 through 5.34 show various layouts for conduit and cable position depending on the section depth and close-coupling options available.


Figure 5.21: Conduit layout: 30 " sections


Figure 5.22: Conduit layout: 34" sections

 -
Figure 5.23: Conduit layout: 38 " sections

Main-tie-main / Close-coupled to transformer / With transition / Additional feeder sections as required


Main-tie-main / Close-coupled to transformer / With transition / Additional feeder sections as required


Figure 5.24: Close-coupled to transformer with transition section: Main-Tie-Main

## Notes:

1. All auxiliary compartments have shallow depths. Device-mounting space on door and rear barrier only.
2. Transition to transformer required with liquid-filled transformed and recommended with dry type transformers. If transition is not used, then space must be provided in the breaker sections for auxiliary devices (PT, CPT, fuses, meters, etc.).

Main-tie-main / close-coupled to transformer / With transition / additional feeder sections as required


Main-tie-main / Close-coupled to transformer / With transition / Additional feeder sections as required


Figure 5.25: Close-coupled to transformer with transition section: Main-Tie-Main and Main-Tie-Tie-Main
Notes:

1. All auxiliary compartments have shallow depths. Device-mounting space on door and rear barrier only.
2. Transition to transformer required with liquid-filled transformed and recommended with dry type transformers. If transition
is not used, then space must be provided in the breaker sections for auxiliary devices (PT, CPT, fuses, meters, etc.).

Main-tie-main / Close-coupled to transformer / With transition / Additional feeder sections as required


Main-tie-main / close-coupled to transformer /
With transition / Additional feeder sections as required


Figure 5.26: Cable or busway connected: Main-Tie-Main
Notes:

1. All auxiliary compartments have shallow depths. Device-mounting space on door and rear barrier only.
2. Transition to transformer required with liquid-filled transformed and recommended with dry type transformers. If transition is not used, then space must be provided in the breaker sections for auxiliary devices (PT, CPT, fuses, meters, etc.).

Main-tie-main / Close-coupled to transformer / With transition / Additional feeder sections as required


Main-tie-main / Close-coupled to transformer /
With transition / Additional feeder fections as required


Figure 5.27: Cable or busway connected: Main-tie-tie-main

## Notes:

1. All auxiliary compartments have shallow depths. Device-mounting space on door and rear barrier only.
2. Transition to transformer required with liquid-filled transformed and recommended with dry type transformers. If transition is not used, then space must be provided in the breaker sections for auxiliary devices (PT, CPT, fuses, meters, etc.).

Main-tie-main / Close-coupled to transformer / With transition / Additional feeder sections as required


Main-tie-main / Close-coupled to transformer / With transition / Additional feeder sections as required


Figure 5.28: 5000 A , Main-tie-main


Figure 5.29: NEMA 1 indoor side view and anchoring details ${ }^{(1)}-\mathrm{in}$. (mm)

| Busway section width required |  |
| :---: | :---: |
| Type and amp rating | Min. section width |
| Spectra | 22.00 in |
| 800 A - 3200 A | ( 558 mm ) |
| Spectra | 30.00 in |
| 4000 A | ( 762 mm ) |
| Spectra | 38.00 in |
| 5000 A | ( 965 mm ) |
| NSP | 22.00 in |
| 1200 A-2500 A | ( 558 mm ) |
| NSP | 30.00 in |
| 3200 A | ( 762 mm ) |
| NSP | 38.00 in |
| 4000 A - 5000 A | (965 mm) |


|  |  |  |  |  |  |  |  |  | Busway locations |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | B | D | G |  |  |  | Front |  |  | Rear |
| Equipment depth | Breaker compartment | Anchor bolt spacing | Back of hoist to rear frame | Spectra 800 A - 4000 A NSP 1200 A - 3200 A | $\begin{array}{r} \text { NSP } \\ 4000 \mathrm{~A} \end{array}$ | $\begin{array}{r} \text { Spectra } \\ 5000- \\ 6000 \mathrm{~A} \end{array}$ | $\begin{aligned} & \text { Spectra } \\ & 800 \mathrm{~A}- \\ & 4000 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} \text { NSP } \\ 1200 \mathrm{~A} \\ -4000 \mathrm{~A} \end{array}$ | $\begin{array}{r} \text { Spectra } \\ 5000 \mathrm{~A} \end{array}$ | $\begin{array}{r} \text { NSP } \\ 5000 \mathrm{~A} \end{array}$ |
| $\begin{aligned} & 54.00 \mathrm{in} \\ & (1372 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 17.00 \mathrm{in} \\ & (432 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 56.00 \mathrm{in} \\ & (1422 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 23.34 \mathrm{in} \\ & (593 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 12.50 \mathrm{in} \\ (317 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 12.50 \mathrm{in} \\ (317 \mathrm{~mm}) \end{array}$ | - | - | - | - | - |
| $\begin{aligned} & 60.00 \mathrm{in} \\ & (1524 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 17.00 \mathrm{in} \\ & (432 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 62.00 \mathrm{in} \\ & (1575 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 29.34 \mathrm{in} \\ & (745 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 21.50 \mathrm{in} \\ (546 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 19.50 \mathrm{in} \\ (495 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 23.50 \mathrm{in} \\ (596 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 9.50 \mathrm{in} \\ (241 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 12.50 \text { in } \\ (317 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 11.50 \mathrm{in} \\ (292 \mathrm{~mm}) \end{array}$ | - |
| $\begin{aligned} & 67.00 \mathrm{in} \\ & (1701 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 17.00 \mathrm{in} \\ & (432 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 69.00 \mathrm{in} \\ & (1752 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 36.34 \mathrm{in} \\ & (923 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 28.50 \mathrm{in} \\ (723 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 26.50 \mathrm{in} \\ (673 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 30.50 \mathrm{in} \\ (774 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 16.50 \mathrm{in} \\ (419 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 12.50 \mathrm{in} \\ (317 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 18.50 \mathrm{in} \\ (470 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 15.88 \mathrm{in} \\ (403 \mathrm{~mm}) \end{array}$ |
| $\begin{aligned} & 74.00 \mathrm{in} \\ & (1879 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 17.00 \mathrm{in} \\ & (432 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 76.00 \mathrm{in} \\ & (1930 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 43.34 \mathrm{in} \\ & (1100 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 35.50 \mathrm{in} \\ (901 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 33.50 \mathrm{in} \\ (850 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 37.50 \mathrm{in} \\ (952 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 23.50 \mathrm{in} \\ (596 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 19.50 \mathrm{in} \\ (495 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 25.50 \mathrm{in} \\ (648 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 22.88 \mathrm{in} \\ (581 \mathrm{~mm}) \\ \hline \end{array}$ |

[^14]
-
Figure 5.30: NEMA 1 indoor floor plan and cable space details ${ }^{(1)}-$ in. (mm)

| A <br> Equipment depth | Direction of cables | J | Rear extension depth | P Transformer $\mathbb{C}$ (center line) to rear of switchgear |
| :---: | :---: | :---: | :---: | :---: |
| 54 in | Below | $19.00 \mathrm{in} \mathrm{(482} \mathrm{mm)}$ | - | $26.50 \mathrm{in} \mathrm{(673} \mathrm{mm)}$ |
|  | Above | 24.00 in ( 609 mm ) |  |  |
| 60 in | Below | 25.00 in ( 635 mm ) | 6.00 in (153 mm) | 26.50 in (673 mm) |
|  | Above | 30.00 in ( 762 mm ) |  |  |
| 67 in | Below | 32.00 in ( 813 mm ) | 13.00 in (330 mm) | 33.50 in (861 mm) |
|  | Above | 37.00 in ( 940 mm ) |  |  |
| 74 in | Below | $39.00 \mathrm{in} \mathrm{(991} \mathrm{mm)}$ | 20.00 in (508 mm) | 40.50 in (1029 mm) |
|  | Above | 44.00 in (1118 mm) |  |  |
| 67 in 5000A, 6000A, 8000A bus | Below | 26.00 in ( 660 mm ) | 7.00 in ( 177 mm ) | $33.50 \mathrm{in}(861 \mathrm{~mm})$ |
|  | Above | 31.00 in ( 787 mm ) |  |  |
| 74 in 5000A, 6000A, 8000A bus | Below | 33.00 in ( 838 mm ) | 14.00 (356 mm) | 40.50 in (1029 mm) |
|  | Above | 38.00 in (965 mm) |  |  |



Figure 5.31: NEMA 3R outdoor non-walk-in side view and anchoring details ${ }^{(1)}$ - in. (mm)


1. Refer to installation drawing and AKD-20 Installation Manual (DEH-41472) for additional information.
2. Customer-supplied equipment required for seismic anchor; recommended for all others.
3. Four (4) anchor clips supplied with switchgear.
4. 5000 A busway to main bus only.
5. Uppermost breaker not available.
6. $800 \mathrm{~A}-2000 \mathrm{~A}$ breaker may be installed in bottom compartment of 30 in . wide sections.


- 

Figure 5.32: NEMA 3R outdoor non-walk-in floor plan and space details ${ }^{(1)}$ - in. (mm)

| Section width | K | N | Indoor frame | L | M | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 24 \mathrm{in} \\ & (609 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 19.25 \mathrm{in} \\ (489 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 16.00 \mathrm{in} \\ (406 \mathrm{~mm}) \end{array}$ | $\begin{aligned} & 60 \mathrm{in} \\ & (1524 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 4.88 \mathrm{in} \\ (124 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 19.00 \mathrm{in} \\ (483 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 32.50 \mathrm{in} \\ (826 \mathrm{~mm}) \end{array}$ |
| $\begin{aligned} & 32 \mathrm{in} \\ & (812 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 27.25 \mathrm{in} \\ (692 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 24.00 \mathrm{in} \\ (609 \mathrm{~mm}) \end{array}$ | $\begin{aligned} & 74 \mathrm{in} \\ & (1879 \mathrm{~mm})^{2} \end{aligned}$ | $\begin{array}{r} 18.88 \mathrm{in} \\ (479 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 33.00 \mathrm{in} \\ (838 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 46.50 \mathrm{in} \\ (1181 \mathrm{~mm}) \end{array}$ |
| $\begin{aligned} & 40 \mathrm{in} \\ & (1016 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 35.25 \mathrm{in} \\ (895 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 32.00 \mathrm{in} \\ (812 \mathrm{~mm}) \end{array}$ | $\begin{aligned} & 74 \mathrm{in} \\ & (1879 \mathrm{~mm})^{3} \end{aligned}$ | $\begin{array}{r} 18.88 \mathrm{in} \\ (479 \mathrm{~mm}) \end{array}$ | $\begin{gathered} 26.00 \mathrm{in} \\ (660 \mathrm{~mm}) \end{gathered}$ | $\begin{array}{r} 40.50 \mathrm{in} \\ (1029 \mathrm{~mm}) \end{array}$ |

[^15]

Figure 5.33: NEMA 3R outdoor walk-in protected aisle side view and anchoring details ${ }^{(1)}-$ in. (mm))

| A <br> Depth of indoor switchgear | D <br> Anchor bolt spacing | E <br> Depth of outdoor switchgear | F <br> Sub base depth | Main bus busway locations Front rear spectra | Busway locations |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Front |  | Rear |
|  |  |  |  |  | $\begin{array}{r} \hline \text { Spectra } 800 \\ A-4000 A \end{array}$ | NSP | Spectra | Spectra |
|  |  |  |  |  | NSP 1200 A - 3200 A | 4000 A | 5000-6000 A | 800 A-4000 A |
| 60.00 in | 106.00 in | 107.62 in | 104.62 in | $\leq 4000 \mathrm{~A}$ | 23.00 in | 21.00 in | - | 11.00 in |
| (1524 mm) | ( 2692 mm ) | ( 2733 mm ) | ( 2657 mm ) |  | (584 mm) | ( 533 mm ) |  | (279 mm) |
| $\begin{aligned} & 74.00 \mathrm{in} \\ & (1880 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 120.00 \mathrm{in} \\ & (3048 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 121.62 \mathrm{in} \\ & (3089 \mathrm{~mm}) \end{aligned}$ | $\begin{aligned} & 118.62 \mathrm{in} \\ & (3012 \mathrm{~mm}) \end{aligned}$ | $\leq 4000 \mathrm{~A}$ | 37.00 in | 35.00 in | - | 25.00 in |
|  |  |  |  |  | (939 mm) | ( 889 mm ) |  | (635 mm) |
|  |  |  |  | 5000 - | 37.00 in | 35.00 in | 37.50 in | 25.00 in |
|  |  |  |  | 6000 A | (939 mm) | (889 mm) | (952 mm) | ( 635 mm ) |

[^16]

Figure 5.34: NEMA 3R outdoor walk-in protected aisle floor plan and cable space details ${ }^{(1)}$ - in. (mm)

| Section width | K | N | Indoor frame | L | M | P |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 22.00 \mathrm{in} \\ & (558 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 19.25 \mathrm{in} \\ (489 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 16.00 \mathrm{in} \\ (406 \mathrm{~mm}) \end{array}$ | $\begin{aligned} & \hline 60 \text { in } \\ & (1524 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 4.88 \mathrm{in} \\ (124 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 19.00 \mathrm{in} \\ (483 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 32.50 \mathrm{in} \\ (826 \mathrm{~mm}) \end{array}$ |
| $\begin{aligned} & 30.00 \mathrm{in} \\ & (762 \mathrm{~mm}) \end{aligned}$ | $\begin{array}{r} 27.25 \mathrm{in} \\ (692 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 24.00 \mathrm{in} \\ (609 \mathrm{~mm}) \end{array}$ | $\begin{aligned} & 74 \mathrm{in} \\ & (1879 \mathrm{~mm})^{2} \end{aligned}$ | $\begin{array}{r} 18.88 \mathrm{in} \\ (479 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 33.00 \mathrm{in} \\ (838 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 46.50 \mathrm{in} \\ (1181 \mathrm{~mm}) \end{array}$ |
| $\begin{aligned} & 38.00 \mathrm{in} \\ & (965 \mathrm{~mm}) \\ & \hline \end{aligned}$ | $\begin{array}{r} 35.25 \mathrm{in} \\ (895 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 32.00 \mathrm{in} \\ (812 \mathrm{~mm}) \\ \hline \end{array}$ | $\begin{aligned} & 74 \mathrm{in} \\ & (1879 \mathrm{~mm})^{3} \\ & \hline \end{aligned}$ | $\begin{array}{r} 18.88 \mathrm{in} \\ (479 \mathrm{~mm}) \\ \hline \end{array}$ | $\begin{array}{r} 26.00 \mathrm{in} \\ (660 \mathrm{~mm}) \end{array}$ | $\begin{array}{r} 40.50 \mathrm{in} \\ (1029 \mathrm{~mm}) \\ \hline \end{array}$ |

[^17]
## Arc-resistant switchgear

ABB AKD-20 and Entellisys arc-resistant (AR) switchgear solutions are for applications where an extra margin of safety is essential. They meet the IEEE C37.20.7 Type 2B AR standard which states that the equipment will provide arcresistance protection on the front, rear, and sides while opening designated low voltage compartments.

Designated compartments include front auxiliary, and instrumentation cubicles. AKD-20 AR and Entellisys AR are designed to contain and redirect the arc flash energy and exhaust gases through the plenum at the top of the enclosure and away from the operator. In the case of an arc flash event, normally open pressure activated flaps close shut to seal ventilation areas in the rear cable compartment.

The rugged dead front panels protect personnel from the explosive force of arc flash occurrences. The circuit breaker cubicle doors are provided with a reinforced escutcheon gasket, protecting operators from exhaust gases and other materials. Arc-resistant AKD-20 and Entellisys are designed with the safety of personnel and equipment in mind. AR is offered in the same shallower footprint as our traditional switchgear. Combine AR with unique GE Entellisys and ArcWatch technologies for even more advanced safety solutions against arc flash occurrences. Using interlocking systems, these two technologies increase protection while maintaining system uptime.

## AR features

- Internal exhaust chimney and exhaust plenums with top, bottom, left, and right exit options
- Seismic construction
- Heavy-duty NEMA 1 enclosure
- Same footprint as standard AKD-20 and Entellisys
- Insulated/Isolated bus
- Bus compartment barriers
- Section barriers and shutters
- Push-to-latch circuit breaker cubicle doors
- Normally open pressure activated rear vent flaps
- Reinforced circuit breaker escutcheon gasket
- Plenum flange
- Full height hinged and bolted rear doors
- Floor plates in cable compartment
- ArcWatch compatible (ABB Pub DEA-565A)


## Ratings

- System voltage nominal (max): 480 (508) V - 600 (635) V
- Main bus: 800 A - 5000 A (5000 A breakers require fan cooling)
- Enclosure type: Indoor NEMA 1
- Depths: 54", 60", 67", and 74"
- Internal arc current: 65 kA (85 kA - consult factory) RMS at 0.5 sec
- Cable-connected or transformer close coupled main and cable-connected feeder breakers


## Standards and approvals

- IEEE C37.20.7 - Type 2B
- ANSI C37.20.1
- UL 1558, UL1066


## Additional reference publications

- DEH-41473 Installation and Maintenance Manual
- DEH-41474 Plenum Installation and Maintenance Manual


## Additional options

- Infrared scanning window in rear doors
- Lockable T-Handles on circuit breaker cubicle
- Doors and rear doors
- Overhead circuit breaker lifting device


## Additional options

AKD-20 or Entellisys Arc-resistant switchgear is provided in NEMA 1 indoor construction for electrical systems rated up to $5000 \mathrm{~A}, 600 \mathrm{~V}$, 65 kA. AKD-20 or Entellisys Arc Resistant switchgear meets the requirements of the following IEEE and UL standards:

- IEEE C37.20.1 (2002) Metal-enclosed low voltage power circuit breaker switchgear;
- IEEE C37.20.7 (2007) Guide for testing metal-enclosed switchgear for internal arcing Faults (tested to Type 2B requirements);
- UL1558 Metal-enclosed low voltage power circuit breaker switchgear.

AKD-20 or Entellisys Arc-resistant switchgear is provided with a plenum flange on the top of each vertical section (refer to conduit/floorplan details provided in this document). The plenum flange at the end of our equipment mates with the ownersupplied plenum (Figure 6-11).
$A B B$ will provide the following relative to the plenum:

1. Details on the minimum material thickness for the plenum;
2. Details on the minimum cross-section of the plenum (minimum ceiling height: 10 ft .);
3. Details on the mating plenum flange on the top of each vertical section;
4.Exhaust port with rodent screen and hinged flap for use on the exiting end of the plenum provided by ABB.

Cubicles with provisions for future circuit breakers are provided with a cover plate in the circuit breaker door cutout and a cassette barrier behind the door. All circuit breaker cubicle doors are provided with a "push-to-latch" mechanism, which eliminates the need for any additional motions to secure the circuit breaker door - a critical factor in maintaining the Type 2B arc-resistant rating of the equipment.

## Arc-resistant type 2B - what does it mean?

 Per IEEE C37.20.7-2007, clause 4.1, "Accessibility Type," the Type designation refers to the placement of the cotton indicators used during testing of the equipment. Type 2 equipment is tested with cotton indicators placed on all four sides (front, back, left end, right end) of the test sample. Suffix "B," as in Type 2B, is explained in IEEE C37.20.7-2007, Annex A. 2 and is given to equipment "where normal operation...involves opening the door or cover of compartments specifically identified as lowvoltage control or instrumentation compartments."Annex A.2.1 reads,
Suffix B testing requires the placement of indicators directly in front of the low voltage control or instrument compartment(s) adjacent to the compartment in which the arc is initiated with the compartment cover/door(s) removed to evaluate entrance of ionized gases into those compartments.

The Type 2B designation does not imply that the switchgear can be operated with the breaker cubicle doors or the hinged rear doors for the cable and bus compartments opened or removed, nor that the switchgear can be operated continuously with the doors for the metering or auxiliary compartments open. Reference IEEE C37.20.7-2007 IEEE, "Guide for Testing Metal-enclosed Switchgear Rated up to 38 kV for Internal Arcing Faults," for full details.

## Cubicle doors - dead front construction

The circuit breaker cubicle doors are provided with a reinforced escutcheon gasket that protects operators by redirecting the arc flash energy and exhaust gases through the plenum at the top of the enclosure. Each circuit breaker compartment door is provided with two self-latching mechanisms with a single "T" shaped door handle (Figure 6.2).

Behind the circuit breaker compartment door is a dead front gasket (Figure 6-5). When the compartment door is closed, the combination of the dead front gasket and the breaker door gasket provides the necessary sealing for the arc-resistant rating (Figure 6.1).


Figure 6.1: Breaker compartment door (closed)

Warning: The breaker compartment door must be closed and latched to maintain the integrity of the arc resistant enclosure. The breaker compartment door should not be opened when the circuit breaker is closed and in the connected position when the equipment is energized.

## Compartment handle

T-handles are standard on all cubicle doors. Key lockable handles (Figure 6.2) are optional. To open the door, rotate the handle clockwise to release the latch mechanisms and pull the door outward. Operating the handle is not necessary to close the door. Simply close the door and push on the door directly behind each latching mechanism (Figure 6.3). Confirmation of the door's being latched can be achieved by pulling on the T-shaped handle while not rotating the handle. If a circuit breaker is to be removed from its compartment for an extended period of time, it is strongly recommended that a future breaker door cover (Figure 6.4) and future breaker cassette barrier (Figure 6.5) be installed to keep any potential electrical arcing events contained within the equipment. Refer to DEH-41473 for future cassette and door covers.


Figure 6.2: Compartment T-handle


Figure 6.3: Breaker compartment door (open)

## Breaker compartment for future circuit breakers

When specified, compartments may be supplied for future addition of circuit breaker elements. These compartments are fully equipped with drawout rails, primary disconnects, and ancillary devices as required (e.g., secondary disconnects, accessory devices, etc.). The opening in the breaker compartment door and the opening in the cassette of the compartment are closed with bolted-on steel plates to deter accidental contact with energized electrical circuits (i.e., primary disconnect stab tips) and provide the necessary structural barriers to achieve the arc resistant rating (Figure 6.4 and Figure 6.5).


Figure 6-4: Future breaker compartment door (closed)


[^18]
## Rear doors

The standard full-height, hinged and bolted rear doors are shown in Figure 6.6. Doors are secured with bolts on both the hinge side and non-hinge side.


Figure 6.6: Bolted rear doors

## Rear compartment features

Figure 6.7 and Figure 6.8 show the pressureactivated rear vent flaps for upper and lower vent openings. Normally held open by gravity, they seal the rear vent openings during an arcing fault. Insulated horizontal main bus, phase isolated vertical riser bus, and barriers between sections in the cable and bus compartments are optional design features. Insulated horizontal main bus, phase isolated vertical riser bus, and barriers between sections in the cable and bus compartments are optional design features.


[^19]

Figure 6.8: Rear vent flaps (bottom)

Steel stiffeners as shown in in Figure 6.9 come standard on rear section doors wider than 30 in.


Figure 6.9: Rear door steel stiffene

Figure 6.10 shows the removable floor plates that are standard design for the cable compartment.


Figure 6.10: Floor plates

## Plenum features

Figure 6.11, Figure 6.12, and Figure 6.13 depict a typical plenum system. The plenum at the top of the enclosure directs the arc flash energy and exhaust gases away from the operator.


Figure 6.11: Exhaust plenum system (front view)

Individual plenum sections extending beyond the end of the switchgear, and end caps are provided by a third-party vendor. Their design is based on ABB plenum specifications. Plenum requirements include 23-gauge min. zinc-plated or painted steel, 12 " x 20 " inside dimensions.


Figure 6.12: Plenum end cap and flange

The vent flap is raised in Figure 6.13 to show the rodent screen built into the plenum exhaust end assembly.


Each section (Figure 6.14) of plenum above the switchgear features a plenum flange and access panel for each vertical section.

## Common plenum

A single plenum system can be used to connect multiple LV switchgear lineups, which allows for a single external exhaust vent, resulting in a simplified installation and reduced space requirements.


[^20]
## Exhaust plenum end portal

The exhaust plenum end portal should be located on an exit wall and secured to this structure. If the exit point of the equipment is an exterior wall, the securing of the exhaust end portal must include methods to prevent water ingress between the portal and a structure wall. Care and consideration should be taken when selecting the exhaust end portal location. An area of at least 10 ft . in all directions from the exhaust end portal needs to be clear of obstructions and access to this area should be restricted for safety. The plenum exhaust end assembly with vent flap is furnished by ABB. Vent flap shown in the closed position in Figure 6.15.


Figure 6.15: Plenum vent

## Portal

Construction of the exhaust plenum between the end flange on the switchgear and the exhaust end portal can vary upon the customer's construction requirements. Care should be taken to ensure that minimum crosssectional area of the exhaust plenum interior volume be 12 in . by 20 in . The exhaust plenum should be constructed of a corrosionresistant metal with a material thickness of no less than 23 gauge.

Total length of the plenum has no restriction. Elevation changes and turns of no greater than $90^{\circ}$ are acceptable, but should be kept to a minimum. Figures 6.16 through 6.17 show the front dimensional vier and cross-sectional view of AR low voltage switchgear.

Notice: The minimum unobstructed ceiling height,from the base of the switchgear is 10 ft . to install the exhaust plenum system.


Figure 6.16: Outline of typical AR low voltage switchgear (front view, in inches)

1. Exhaust plenum section, 38 in. stack
2. Exhaust plenum section, 30 in. stack
3. Exhaust plenum section, 22 in. stack
4. Transition adaptor section (typical)
5. End cap
6. Exhaust plenum end portal
7. Exhaust plenum access cover (typical)


Figure 6.17: Cross-sectional view of AR low voltage switchgear

Figure 6.18 shows a typical indoor enclosure floor plan and cable entry space. Table 6.1 shows the enclosure depths, cable direction, and cable space for AKD-20 AR and Entellisys AR.

- Note 1: Offset ground bus. If greater than six ground lugs are required in the same section, an offset ground bus is provided. When the offset ground bus and cable entry are located both bottom or above, it will reduce the available cable space.
- Note 2: Neutral bus (optional, AKD-20AR only). When this option is provided and the neutral bus and cable entry is located both at bottom or top, it will reduce the available cable space.
- Note 3: Neutral bus (optional, Entellisys AR only). When this option is provided and the neutral bus and cable entry are located both at bottom or top, it will reduce the available cable space.
- Note 4: Cable direction below. If the section does not have a circuit breaker in the "D" compartment, an additional 4 in . of cable space is available.


Figure 6.18: Indoor enclosure floor plan and cable entry space (in inches)

- General: Secondary control lead space may be required on left, right, or both sides of the cable compartment. Consult factory drawings for details.

Table 6.1: Indoor enclosure depth, cable direction, and cable space (in inches)


Figures 6.19 and 6.20 show a typical side view of AKD-20 AR with reference Table 6.2 for dimensions. Figure 6.21 shows the outline of typical AR door features.


Figure 6.19: Outline of typical AR low voltage switchgear (side view)

Table 6.2: Arc-resistant low voltage switchgear assembly depths (in inches)

| Dimension |  |  | Depth |  |
| :--- | ---: | ---: | ---: | ---: |
| C | 24.74 | 24.74 | 37.74 | 44.74 |
| D | 54 | 60 | 67 | 74 |



Figure 6.20: Outline of typical AR low voltage switchgear (side view)

Warning: The breaker compartment door must be closed and latched to maintain the integrity of the arc resistant enclosure. The breaker compartment door should not be opened when the circuit breaker is closed and in the connected position when the equipment is energized.


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Cary，NC 27511
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[^0]:    1. Servicing consists of adjusting, cleaning, lubricationg, tightening, etc. as recommended by the manufacturer. When current is interrupted, dressign of contacts may be required as well. The operations listed are on the basis of servicing at intervals of six months or less.
    2. With closing and opening currents up to the continuous current rating of the circuit breaker at voltages up to the rated maximum voltage ( $85 \%$ or higher power factor).
    3. The number of operations was determined with closing currents up to $100 \%$ ( $80 \%$ power factor or higher) of the continuous current rating of the circuit breaker at voltages up to the rated maximum voltage. With closing and opening currents up to $600 \%$ ( $50 \%$ power factor or less) of the continuous current rating of the circuit breaker at voltages up to rated maximum voltage, the number of operations shown should be reduced to $10 \%$ of the number listed in the column.
    4. If a fault operation occurs before the completion of the listed number of operations, servicing is recommended and possible functional part repmacement may be necessary depending on previous accumulated duty, fault magnitude, and expected future operations
[^1]:    Figure 1.7: Rack padlocked

[^2]:    Figure 1.14: Remote racking controlle

[^3]:    Figure 1-17: Overhead hoist

[^4]:    - Spring charge time $=3 \mathrm{sec}$ max.
    - Duty cycle $=2 / \mathrm{min}$.
    - Envelope 1 motors: running VA ~ 300 VA; inrush $=2$ to 3 times.
    - Envelope 2 and 3 motors: running VA $\sim 450$ VA; inrush $=2$ to 3 times

[^5]:    Figure 2.12: Time delay module

[^6]:    - Position switch contact ratings - 0.5 A @125 Vdc, $0.25 \mathrm{~A} @ 250 \mathrm{Vdc}, 10.0 \mathrm{~A} @ 120 \mathrm{Vac} / 240 \mathrm{Vac}$

[^7]:    Figure 2.16: EntelliGuard G Breaker - Typical control circuits

[^8]:    1. Example: GA16E is EntelliGuard G, $1600 \mathrm{~A}, 85 \mathrm{kA}$ interrupting

    85 kA withstand, Envelope 2.
    2. Refer to Table 2.3: ANSI/UL1066 LVPCB
    interrupting ratings.

[^9]:    1. Main breaker sized for transformer base kVA. (Larger main breaker is sized for transformers with dual temperature rise and/or forced air cooling.)
    2. Main breaker is Envelope 2 or 3 to accommodate ground fault CTs for 4 -wire multi-source ground fault protection.
    3. Main breaker has 30 cycle withstand rating (ICW) greater than transformer maximum short circuit current (ISC)
    4. Equipment ANSI short circuit rating is based on the breaker (main or feeder) with the lowest short circuit rating (ICU).
    5. ICW = 30 cycle withstand current rating; ICU = maximum short circuit interrupting rating; ISC = available short circuit current.
    6. Arc flash incident energy calculated at fault current based on minimum Z\% and full motor contribution. 600 V , resistance grounded or floating system, arc in a box 32 mm arcing gap and 18 " working distance. Circuit breaker clearing time is 3 cycles (instantaneous).
    7. Arc flash incident energy may be calculated using different assumptions. IEEE 1584 has been used as the guide for the above calculated incident energy values
[^10]:    1. Main breaker sized for transformer base kVA. (Larger main breaker is sized for transformers with dual temperature rise and/or forced air cooling.)
    2. Main breaker is Envelope 2 or 3 to accommodate ground fault CTs for 4 -wire multi-source ground fault protection.
    3. Main breaker has 30 cycle withstand rating (ICW) greater than transformer maximum short circuit current (ISC).
    4. Equipment ANSI short circuit rating is based on the breaker (main or feeder) with the lowest short circuit rating (ICU).
    5. ICW = 30 cycle withstand current rating; ICU = maximum short circuit interrupting rating; ISC = available short circuit current.
    6. Arc flash incident energy calculated at fault current based on minimum $\mathrm{Z} \%$ and full motor contribution. $\mathbf{4 8 0} \mathrm{V}$, resistance grounded or floating system, arc in a box,

    32 mm arcing gap and 18 " working distance. Circuit breaker clearing time is 3 cycles (instantaneous).
    7. Arc flash incident energy may be calculated using different assumptions. IEEE 1584 has been used as the guide for the above calculated incident energy values.

[^11]:    1. Main breaker sized for transformer base kVA. (Larger main breaker is sized for transformers with dual temperature rise and/or forced air cooling.)
    2. Main breaker is Envelope 2 or 3 to accommodate ground fault CTs for 4 -wire multi-source ground fault protection.
    3. Main breaker has 30 cycle withstand rating (ICW) greater than transformer maximum short circuit current (ISC).
    4. Equipment ANSI short circuit rating is based on the breaker (main or feeder) with the lowest short circuit rating (ICU).
    5. ICW = 30 cycle withstand current rating; ICU = maximum short circuit interrupting rating; ISC = available short circuit current.
    6. Arc flash incident energy calculated at fault current based on minimum $\mathrm{Z} \%$ and $50 \%$ motor contribution. 240 V , resistance grounded or floating system, arc in a box,

    32 mm arcing gap and 18 " working distance. Circuit breaker clearing time is 3 cycles (instantaneous).
    7. Arc flash incident energy may be calculated using different assumptions. IEEE 1584 has been used as the guide for the above calculated incident energy values.

[^12]:    1. Main breaker sized for transformer base kVA. (Larger main breaker is sized for transformers with dual temperature rise and/or forced air cooling.)
    2. Main breaker is Envelope 2 or 3 to accommodate ground fault CTs for 4 -wire multi-source ground fault protection.
    3. Main breaker has 30 cycle withstand rating (ICW) greater than transformer maximum short circuit current (ISC).
    4. Equipment ANSI short circuit rating is based on the breaker (main or feeder) with the lowest short circuit rating (ICU).
    5. $I C W=30$ cycle withstand current rating; ICU = maximum short circuit interrupting rating; ISC = available short circuit current.
    6. Arc flash incident energy calculated at fault current based on minimum Z\% and $50 \%$ motor contribution. 240 V , resistance grounded or floating system, arc in a box,

    32 mm arcing gap and 18 " working distance. Circuit breaker clearing time is 3 cycles (instantaneous).
    7. Arc flash incident energy may be calculated using different assumptions. IEEE 1584 has been used as the guide for the above calculated incident energy values.

[^13]:    Figure 4.1: Entellisys architecture overview

[^14]:    1. Refer to installation drawing and AKD-20 Installation Manual (DEH-41472) for additional information.
    2. Customer-supplied equipment required for seismic anchor; recommended for all others.
    3. Typical extension of instrumentation on front of section.
    4. Uppermost breaker not available when used with a 4 in . subframe or housekeeping pad.
[^15]:    1. Refer to installation drawing and AKD-20 Installation Manual (DEH-41472) for additional information.
    2. 14 in. rear extension. Main bus $\leq 4000 \mathrm{~A}$.
    3. 5000A, 6000 A , and 8000 A bus without 5000 or 6000 A breaker, 7 in . rear extension
[^16]:    1. Refer to installation drawing and AKD-20 Installation Manual (DEH-41472) for additional information.
    2. Customer-supplied equipment required for seismic anchor; recommended for all others.
    3. Four (4) anchor clips supplied with switchgear.
    4. $800 \mathrm{~A}-2000 \mathrm{~A}$ breaker may be installed in bottom compartment of 30 in . wide sections only.
[^17]:    1. Refer to installation drawing and AKD-20 Installation Manual (DEH-41472) for additional information.
    2. 14 in. rear extension. Main bus $\leq 4000 \mathrm{~A}$.
    3. 5000A, 6000 A , and 8000 A bus without 5000 or 6000 A breaker, 7 in. rear extension
[^18]:    Figure 6.5: Future breaker compartment door (open)

[^19]:    Figure 6.7: Rear vent flaps (top)

[^20]:    Figure 6.14: Plenum rodent screen

